

428 Rec'd PCT/PTO 29 DEC 1999

FORM PTO-1390
(REV 10-94)

U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

ATTORNEY'S DOCKET NUMBER

TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371

9320.92USWO

U.S. APPLICATION NO. (If known, see 37 C.F.R. 1.5)

Unknown 09/446958

INTERNATIONAL APPLICATION NO.

PCT/FR98/01398

INTERNATIONAL FILING DATE

June 30, 1998

PRIORITY DATE CLAIMED

July 1, 1997

TITLE OF INVENTION

MULTICARRIER MODULATION USING WEIGHTED PROTOTYPE FUNCTIONS

APPLICANT(S) FOR DO/EO/US

COMBELLES et al.

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39(I).
4. ☐ A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☒ has been transmitted by the International Bureau.
 - c. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
6. ☐ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3))
 - a. ☐ are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ have been transmitted by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☒ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☒ An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)).
10. ☐ A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern document(s) or information included:

11. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☒ A FIRST preliminary amendment.
☐ A SECOND of SUBSEQUENT preliminary amendment.
14. ☐ A substitute specification.
15. ☐ A change of power of attorney and/or address letter.
16. ☐ Other items or information:

U.S. APPLICATION NO. (if known, see 37 C.F.R. 1.5) Unknown 09/446958		INTERNATIONAL APPLICATION NO. PCT/FR98/01398		ATTORNEY'S DOCKET NUMBER 9320.92USWO	
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17. <input checked="" type="checkbox"/> The following fees are submitted:				CALCULATIONS PTO USE ONLY	
BASIC NATIONAL FEE (37 CFR 1.492(a) (1)-(5)): Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO.....\$970.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO.....\$840.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO.....\$760.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) but all claims did not satisfy provisions of PCT Article 33(1)-(4)\$670.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(1)-(4)\$96.00					
ENTER APPROPRIATE BASIC FEE AMOUNT =					
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).					
CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE		
Total claims	19 -20 = 0		X \$18.00		
Independent claims	5 -3 = 2		X \$78.00	\$0	\$156.00
MULTIPLE DEPENDENT CLAIM(S) (if applicable)				+ \$260.00	\$0
TOTAL OF ABOVE CALCULATIONS =				\$1126.00	
Reduction by 1/2 for filing by small entity, if applicable. Verified Small Entity Statement must also be filed (Note 37 CFR 1.9, 1.27, 1.28).				\$0	
SUBTOTAL =				\$1126.00	
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				+ \$0	
TOTAL NATIONAL FEE =				\$1126.00	
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property				+ \$0	
TOTAL FEES ENCLOSED =				\$1126.00	
				Amount to be: refunded	\$
				charged	\$


a. ☒ Check(s) in the amount of \$1126.00 to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees.
A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any
overpayment to Deposit Account No. 13-2725.

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:
 John J. Gresens
 MERCHANT & GOULD P.C.
 3100 Norwest Center
 90 South Seventh Street
 Minneapolis, MN 55403


 SIGNATURE:

 John J. Gresens
 NAME

 33,112
 REGISTRATION NUMBER

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

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Applicant: COMBELLES et al.
Docket: 9320.92USWO
Title: MULTICARRIER MODULATION USING WEIGHTED PROTOTYPE FUNCTIONS

CERTIFICATE UNDER 37 CFR 1.10

'Express Mail' mailing label number: EL455019886US

Date of Deposit: December 29, 1999

I hereby certify that this paper or fee is being deposited with the United States Postal Service 'Express Mail Post Office To Addressee' service under 37 CFR 1.10 and is addressed to the Assistant Commissioner for Patents, Washington, D.C. 20231.

By: *Linda McCormick*
Name: Linda McCormick

BOX PATENT APPLICATION
Assistant Commissioner for Patents
Washington, D.C. 20231

Sir:

We are transmitting herewith the attached:

- ☒ Transmittal sheet, in duplicate, containing Certificate under 37 CFR 1.10.
- ☒ National Stage PCT Patent Application: Spec. 28 pgs; 19 claims
The fee has been calculated as shown below in the 'Claims as Filed' table.
- ☒ 13 sheets of formal drawings
- ☒ An unsigned Combined Declaration and Power of Attorney
- ☒ A check in the amount of \$1126.00 to cover the Filing Fee
- ☒ Other: Preliminary Amendment; Form PTO-1390
- ☒ Return postcard

CLAIMS AS FILED

Number of Claims Filed		In Excess of:		Number Extra		Rate		Fee
Basic Filing Fee								\$970.00
Total Claims								
19	-	20	=	0	x	18.00	=	\$0.00
Independent Claims								
5	-	3	=	2	x	78.00	=	\$156.00
MULTIPLE DEPENDENT CLAIM FEE								\$0.00
TOTAL FILING FEE								\$1126.00

Please charge any additional fees or credit overpayment to Deposit Account No. 13-2725. A duplicate of this sheet is enclosed.

MERCHANT & GOULD P.C.
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By: *John J. Gresens*
Name: John J. Gresens
Reg. No.: 33,112
Initials: JJG:tvm

S/N Unknown

PATENT

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant:	COMBELLES et al.	Examiner:	Unknown
Serial No.:	Unknown	Group Art Unit:	Unknown
Filed:	December 29, 1999	Docket No.:	9320.92USWO
Title:	MULTICARRIER MODULATION USING WEIGHTED PROTOTYPE FUNCTIONS		

CERTIFICATE UNDER 37 CFR 1.10

'Express Mail' mailing label number: EL455019886US

Date of Deposit: December 29, 1999

I hereby certify that this correspondence is being deposited with the United States Postal Service 'Express Mail Post Office To Addressee' service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, D.C. 20231.

By:

Name: Linda McCormick

PRELIMINARY AMENDMENT

Box PCT
Assistant Commissioner for Patents
Washington, D. C. 20231

Dear Sir:

In connection with the above-identified application filed herewith, please enter the following preliminary amendment.

IN THE ABSTRACT

The abstract page was not included with the application. The abstract will be provided at a later date.

IN THE CLAIMS

In claim 5, line 22, delete "any of the claims 1 to 4", and insert—to claim 1—

In claim 6, line 24, delete "any of the claims 1 to 5" and insert—claim 1—

In claim 7, line 3, delete "any of the claims 1 to 6" and insert—claim 1—

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In claim 8, line 10, delete "any of the claims 1 to 7" and insert—claim 1—

In claim 13, line 14, delete "any of the claims 11 and 12" and insert—claim 11—

In claim 14, line 18, delete "any of the claims 11 to 13" and insert—claim 11—

In claim 15, line 26, delete "any of the claims 11 to 14" and insert—claim 11—

In claim 18, line 28, delete "any of the claims 16 and 17" and insert—claim 16—

REMARKS

The above preliminary amendment is made to remove multiple dependencies from claims 5, 6, 7, 8, 13, 14, 15 and 18.

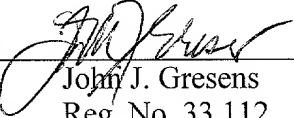
Applicants respectfully request that the preliminary amendment described herein be entered into the record prior to calculation of the filing fee and prior to examination and consideration of the above-identified application.

If a telephone conference would be helpful in resolving any issues concerning this communication, please contact Applicants' primary attorney-of record, John J. Gresens (Reg. No. 33,112), at (612) 371.5265.

Respectfully submitted,

MERCHANT & GOULD P.C.
3100 Norwest Center
90 South Seventh Street
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Dated: December 29, 1999

By 
John J. Gresens
Reg. No. 33,112

13/PRTS

MULTICARRIER MODULATION USING WEIGHTED PROTOTYPE
FUNCTIONS

1 - Field of the Invention

1-1 General Points

5 The field of the invention is that of the transmission or broadcasting of digital data, or of analog and sampled data, designed to be received especially by mobiles. More specifically, the invention relates to the implementation of OFDM/OQAM type multicarrier signals. In other words, the invention applies to density 2 or even higher density signals.

10 It is known that multicarrier modulation has many useful features, especially when it is associated with error-correcting encoding and interleaving. The COFDM (Coded Orthogonal Frequency Division Multiplexing) technique has also been chosen for the European digital audio broadcasting (DAB) standard and for the terrestrial digital video broadcasting (DVB-T).

15 The COFDM technique offers a particularly simple system of equalization, namely the use of a guard interval, also called a cyclical prefix. This cyclical prefix provides for robust behaviour in the face of the echoes but at the cost of a relatively major loss of spectral efficiency.

 This problem is discussed inter alia in the French patent application No. FR-
20 95 05455 (in which the COFDM modulation is called an OFDM/QAM modulation). To overcome this problem, this patent document presents a new technique for the implementation of OFDM/OQAM type multicarrier modulations.

 It will be noted that the different types of modulation discussed hereinafter are designated in a slightly different way in this prior art document and in the present
25 patent application. The following table gives the correspondence :

FR95 05455 :	Present Document:
OFDM/QAM	OFDM/QAM/OFDM
OFDM/OQAM	OFDM/OQAM/NYQUIST

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OFDM/OMSK

OFDM/OQAM/MSK

OFDM/IOTA

OFDM/OQAM/IOTA

The term « OQAM » refers to the « Offset Quadratic Amplitude Modulation » definition. This expresses the fact that, for such modulations, there is a temporal offset between the transmission of the in-phase part and that of the in-quadrature part of a QAM symbol.

5 1-2 Applications

The invention can be applied in very many fields, especially when high spectral efficiency is sought and when the channel is highly non-stationary.

A first category of applications relates to terrestrial digital radio-broadcasting, whether of images, sound and/or data. In particular, the invention can be applied to synchronous broadcasting which intrinsically generates long-term multiple paths. It can also be advantageously applied to broadcasting towards mobile bodies.

Another category of applications relates to digital radiocommunications. The invention can be applied especially in systems of digital communications towards mobiles using high bit rates.

15 **2 - Reminders**

2-1 Transmission channel

In a radiomobile environment, the transmitted wave undergoes multiple reflections, and the receiver therefore receives a sum of versions delayed by the transmitted signal. Each of these versions is attenuated and phase-shifted randomly. Since the receiver is assumed to be in motion, the Doppler effect acts also on each path.

The conjunction of these efforts results in a non-stationary channel with deep fading at certain frequencies (frequency selective channel). For the applications referred to here, the transmission band is greater than the coherence band of the channel (the band for which the frequency response to the channel may be considered to be constant on a given duration), and fading thus appears in the band, i.e. at a given

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point in time, certain frequencies are highly attenuated.

2-2 Description of a multicarrier modulation

A multicarrier modulation is above all a digital modulation, namely a method for the generation of an electromagnetic signal out of the digital information to be transmitted. The originality and value of such a modulation is that it subdivides the limited band allocated to the signal into subbands. In these subbands, which have a chosen width smaller than the coherence band of the channel, the channel may be considered to be constant for a duration of transmission of a symbol, chosen to be smaller than the coherence time of the channel.

The digital information to be transmitted during this period is then distributed over each of these subbands. This has two uses in particular:

- reducing the modulation speed (namely increasing the symbol duration) without modifying the transmitted bit rate,
- simply modelling the action of the channel on each of the subbands: complex multiplier.

It will be noted that, in reception, a system of low complexity for the correction of the data elements received (complex division by the estimated channel) enables a recovery of the information transmitted on each of the carriers satisfactorily except for the carriers that have undergone a deep fading. In this case, if no steps for protecting the information have been taken, the data elements conveyed by these carriers will be lost. A multicarrier system therefore ensures that the generation of the electrical system must be preceded by digital data processing (error corrective encoding and interleaving).

The patent No. FR 95/05455 gives a detailed description of the two types of existing multicarrier modulation. Their characteristics may be briefly recalled here.

2-2-2 Notations

Spacing between two adjacent carriers of the multiplex of carriers: ν_0 .

Temporal spacing between two multicarrier symbols transmitted (symbol

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time): τ_0 .

2-2-3 The prototype function

The shaping filter for each of the carriers of the multiplex is the same. It corresponds to the prototype function characterizing the multicarrier modulation.

- 5 Let $g(t)$ be this prototype function, the signal transmitted at each instant $n\tau_0$, on the m^{th} central frequency subband ν_m , is $a_{m,n} e^{i\varphi_{m,n}} e^{2i\pi\nu_m t} g(t - n\tau_0)$.

In baseband, the expression of the signal transmitted, centered on the frequency $M\nu_0$ is therefore:

10
$$s(t) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} e^{i\varphi_{m,n}} e^{2i\pi m \nu_0 t} g(t - n\tau_0) \quad (1)$$

- The functions $e^{i\varphi_{m,n}} e^{2i\pi m \nu_0 t} g(t - n\tau_0)$ are called time-frequency translated functions of $g(t)$. To retrieve the information transmitted by each of the subcarriers, it is necessary to choose $g(t)$ so that its time-frequency translated functions are
15 separable. To be sure of this, it is laid down that these translated functions should be orthogonal in the sense of a scalar product defined on all the finite energy functions (which is a Hilbert space in the mathematical sense). This space accepts two possible scalar products, namely:

- the complex PS $\langle x|y \rangle = \int_R x(t)y^*(t)dt$
20 - the real PS $\langle x|y \rangle = \Re e \left(\int_R x(t)y^*(t)dt \right)$

Thus two types of multicarrier modulation are defined:

- complex type, or again OFDM/QAM: the function $g(t)$ chosen guarantees an orthogonality of its translated functions in the complex sense (example: OFDM, also called OFDM/QAM/OFDM). In this case, $\varphi_{m,n} = 0$ and the data
25 elements $a_{m,n}$ are complex,
- real type or again OFDM/OQAM: the function $g(t)$ chosen guarantees an

orthogonality of its translated functions in the real sense (examples: OFDM/OQAM/NYQUIST, OFDM/OQAM/MSK, OFDM/OQAM/IOTA).

In this case, $\varphi_{m,n} = (\pi/2) * (m+n)$ and the data elements $a_{m,n}$ are real.

2-2-4 Density of the "time-frequency" network

- 5 Since these modulations are designed for transmission at high bit rates, they will be associated with fairly high spectral efficiency values, in the range of 4 bits/s/Hz (digital television). The mapping of the bits coming from the error correction encoder will thus be of the QAM type.

10 For an OFDM/QAM modulation, the real and imaginary parts of a complex function derived from the QAM constellation are transmitted simultaneously at every symbol time T_s .

In the case of an OFDM/OQAM type modulation, they are transmitted with a temporal offset (QAM offset) of half a symbol time ($T_s/2$). For one and the same transmission band and one and the same number of subcarriers, it is therefore
15 necessary, for one and the same bit rate to be transmitted, that the rate of transmission of OFDM/OQAM type multicarrier symbols should be twice that of the OFDM/QAM type multicarrier symbols.

These two modes of transmission of information are characterized by the density of the time-frequency network $d = 1/(v_0 \tau_0)$. The OFDM/OQAM type
20 multicarrier modulations correspond to a density $d = 2$, and those of the OFDM/QAM type correspond to a density of $d = 1$.

It may be noted that a multicarrier modulation is characterized by:

- the density of the "time-frequency" network on which it is defined,
- the prototype function.

- 25 The implementation of an OFDM/OQAM modulation with a density 2, and of the corresponding demodulation, requires substantial computation power and high storage capacity. This therefore underlines the fact that the corresponding instruments are relatively complex and costly.

3 – Goals of the invention

The invention is designed especially to overcome or reduce these drawbacks. More specifically, a goal of the invention is to provide techniques for the modulation and demodulation of the multicarrier signals that are simple and cost little to implement as compared with the direct approaches.

In other words, it is a goal of the invention to give modulation and demodulation techniques of this kind that limit the number of operations to be performed and the necessary storage capacity.

4 - Description of the invention

- These goals as well as others that shall appear hereinafter are achieved according to the invention by means of a method for the modulation of a multicarrier signal with a density $1/(v_0 \cdot \tau_0) = 2$, formed by successive symbols, each comprising M samples to be transmitted and constituted by a set of 2M orthogonal carrier frequencies in the real sense,
- the interval between two neighboring carrier frequencies being equal to v_0 and the interval between the times of transmission of two consecutive symbols, or the symbol time, being equal to τ_0 ,
- each of said carrier frequencies being modulated according to one and the same modulation prototype function $g(t)$ with a truncation length of $2L\tau_0$,
- the method comprising, at each symbol time, the following steps:
- the obtaining of a set of 2M complex coefficients representing data to be transmitted;
 - the computing of 2LM linear combinations from said 2M complex coefficients obtained, the weighting coefficients used in these combinations representing said prototype function $g(t)$, so as to obtain 2LM coefficients;
 - the summing of said 2LM coefficients weighted in the predetermined storage locations of a memory comprising 2LM storage locations representing 2L groups of M distinct partial sums,

so as to gradually form, in said storage locations, over a duration of $2L\tau_0$, M samples to be transmitted;

- the sending of said samples to be transmitted.

Thus, according to the invention, the data elements to be processed are stored after
5 weighting and not before. It is thus possible to reduce the memory capacity needed as well as the number of operations performed. The samples to be transmitted are built gradually in each field of storage.

According to one advantageous embodiment of the invention, a sample to be transmitted at the instant $j\tau_0 + k\tau_0/M$, referenced s_{k+jM} is written as follows:

10

$$s_{k+jM} = \sum_{q=0}^{2L-1} [\alpha_{k,q} C_{k,j-q} + \beta_{k,q} C_{k+M,j-q}]$$

where:

$C_{0,j}$ to $C_{2M-1,j}$ are the $2M$ complex coefficients generated between the instants
15 $j\tau_0$ and $(j+1)\tau_0$;

$\alpha_{k,q}$ and $\beta_{k,q}$ are said weighting coefficients.

In the case of an OFDM/OQAM modulation, we will generally have:

- $\alpha_{k,q} = 0$ for q as an odd parity number;

- $\beta_{k,q} = 0$ for q as an even parity number.

20 The number of operations performed is therefore further reduced by half.

In a preferred embodiment of the invention, the method comprises, for the generation of a symbol with an index j formed by M samples, the following steps:

- the obtaining of $2M$ real inputs $a_{m,n}$ representing a source signal;

- the pre-modulation of each of said real inputs producing $2M$ complex
25 coefficients;

- the reverse Fourier transform of said $2M$ complex coefficients producing $2M$ complex transform coefficients $C_{0,j}$ to $C_{2M-1,j}$;

- for each of the M pairs $(C_{k,j}, C_{(k+M),j})$ of said transform coefficients, the

computation of $2L$ weighted coefficients, the weighing coefficients representing said prototype function;

- the addition of the result of each of said weighted $2LM$ values to the contents of the $2LM$ distinct memory zones so as to gradually build the samples to be transmitted constituting the symbols $j, (j+1), (j+2), \dots (j+2L-1)$;

- the sending of M samples corresponding to the M oldest contents of said memory zones and then the resetting of the contents of said M memory zones.

In general, said steps will be implemented at the rate τ_0/M of the samples.

The checking of the storage means is very simple. Thus, each sending step may be followed by a step for the updating of said memory locations comprising:

- a physical shifting of the contents of each of said memory locations if the latter are elements of a shift register; or

- an updating of the write and read addresses of said memory locations, if the latter are elements of a RAM.

According to an advantageous characteristic of the invention, said coefficients representing data elements to be transmitted are obtained by the implementation of a mathematical transform comprising the following steps:

- the application of a real reverse Fourier transform;

- the circular permutation of the result of this reverse transform by $M/2$ coefficients leftwards;

- the multiplication of each of said coefficients by i^n .

It is thus possible to obtain complex transform coefficients from an FFT with real inputs. Again, this makes it possible to limit the number of operations performed.

It is furthermore possible to simplify the computations by slightly modifying the equation of the signal centered on the frequency Mv_0 so that it is written as follows:

$$s(t) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} (-1)^{m(n+L)} i^{m+n} e^{2i\pi m v_0 t} g(t - n\tau_0)$$

The invention also relates to the modulation devices implementing a modulation method of this kind.

According to a particular embodiment, this device comprises especially:

- means of mathematical transformation delivering said coefficients representing data elements to be transmitted at the rate $\tau_0/2M$ and in the following order $(C_{0,j}, C_{M+1,j}), \dots, (C_{M-1,j}, C_{2M-1,j})$;
- $2LM-M$ simultaneous read/write RAM type memory locations;
- N complex multipliers working at the rate $N\tau_0/2LM$, N being equal to 1, 2, 4, ... or $2L$.

Thus, the memory space is further reduced.

The invention also relates to a method for the demodulation of a received signal corresponding to a multicarrier emitted signal with a density $1/(\nu_0 \tau_0) = 2$. According to this method, an estimation of $2M$ real data elements transmitted at a given symbol time is reconstituted by means of the following steps:

- the sampling of said signal received at the sample frequency τ_0/M , delivering M complex samples received;
- the storage of each of said M complex samples received in a predetermined location of an input memory comprising $2ML$ complex locations, in which there have been previously memorized $(2L-1)M$ samples received during the $2l-1$ previous symbol times;
- the multiplication of the $2ML$ values contained in said input memory by coefficients representing said prototype function;
- temporal aliasing, by the summing up of $2M$ series of L results of multiplication, so as to obtain $2M$ complex values;
- the processing of said $2M$ complex values to form said estimations of the $2M$ real data elements transmitted.

Advantageously, the $2M$ complex values derived from the temporal aliasing step between the instants $(j+2L-1)\tau_0$ and $(j+2L)\tau_0$ are written as follows:

$$R_{k,j} = \sum_{q'=0}^{2L-1} \alpha'_{k,q} r_{k'+(j+q')M}$$

$$R_{k'+M,j} = \sum_{q'=0}^{2L-1} \beta'_{k,q} r_{k'+(j+q')M}$$

where:

5 $r_{k'+(j+q')M}$ represents the sample received at the instant $k'\tau_0+(j+q')\tau_0/M$;

$\alpha'_{k,q}$ and $\beta'_{k,q}$ are said weighting coefficients.

Most usually, the computations will be simplified because:

- $\alpha'_{k,q'} = 0$ for q' as an odd parity value;
- $\beta'_{k,q'} = 0$ for q' as an even parity value.

10 According to a preferred embodiment, said processing step comprises the following steps:

- the application of a mathematical transformation that is the reverse of the one performed during the modulation on said $2M$ complex values delivering $2M$ transformed values;
- 15 - the correction of phase and/or amplitude distortions due to the transmission channel;
- the extraction of the real part of said transformed complex values.

In general, said steps are implemented at the rate τ_0/M of the samples.

20 The invention also relates to the demodulation devices implementing this method. These devices comprise:

- means for the sampling of said received signal;
- means for the temporary storage of the complex sample functions comprising $2ML$ complex locations;
- means for the multiplication of said memorized samples by weighting
- 25 coefficients representing said prototype function;
- temporal aliasing means summing up L weighting results so as to obtain $2M$

- means for the processing of said complex values delivering an estimation of 2M real data elements transmitted at each symbol time.

5 means of:

- 10

15

comprising the following steps for each series of complex input values:

- 20

- the summing of each of the weighted values in a predetermined memory location out of a set of 2ML memory locations each containing a partial sum so as to gradually form said output values in said memory locations on a period corresponding to the reception of 2L series of complex input values.

25

The term "filtering" must of course be taken here in its general sense of processing or computation performed on data elements. This processing which

comprises the computation of a weighted sum is done gradually.

5 - Description of a preferred embodiment

5-1 List of figures

Other features and advantages of the invention shall appear more clearly from the following description of a preferred embodiment of the invention given as a simple non-restrictive illustration, and from the appended drawings, of which:

- Figure 1 gives a general and simplified illustration of the method of modulation of the invention (step j) used to generate M samples;
- Figure 2 illustrates the gradual construction of the M samples where $L=4$; for the Iota waveform;
- Figure 3 gives a more detailed illustration of the working of the method of modulation of the invention for the instants $j-1$ to $j+2$;
- Figure 4 specifies the initiation of the procedure of modulation of Figure 3 where $L = 4$;
- Figure 5 is a schematic diagram of a complex IFFT circuit known per se;
- Figures 6A to 6C illustrate the optimized architectures implementing FIFO systems and respectively using a single multiplier (Figure 6A), L multipliers (Figure 6B) or $2L$ multipliers (Figure 6C);
- Figure 7 shows an optimized embodiment of the reverse FFT using a real input FFT;
- Figure 8 illustrates the working of the demodulation method of the invention when $L=4$;
- Figure 9 shows the general case of demodulation deduced directly from Figure 8;
- Figure 10 illustrates a corresponding demodulator architecture;
- Figures 11 to 12 show two modes of implementation of the reception filtering in the case of a FIFO structure respectively using L and $2L$

multipliers.

5-2 Notations

- . Intercarrier spacing: ν_0 .
- . Intersymbol duration: τ_0 .
- 5 . Density of the network: $1/(\nu_0\tau_0) = 2$.
- . Band allocated to the signal: $W = 2M\nu_0$.
- . Sampling frequency: $f_e = 1/T_e = M/\tau_0$.
- . Length of truncation of the protocol function: $2L\tau_0$.

10 In theory, the prototype function is the temporal support and/or infinite sequential support. However, to implement the corresponding digital filter, this function must be truncated.

This is the case in OFDM/OQAM/NYQUIST (infinite temporal support) and in OFDM/OQAM/IOTA (infinite temporal and frequency supports). Typically, for the function Iota, $L = 4$ at the minimum. For a
15 sampling at T_e defined here above, the digital function will have the length of $2LM$ real coefficients.

. Indices of the samples:

To be consistent with the formula given hereinafter, the following is
noted:

$$\begin{aligned} x_k &= x\left(k\frac{\tau_0}{M} - L\tau_0\right) \\ x_{k+LM} &= x\left(k\frac{\tau_0}{M}\right) \end{aligned} \quad (2)$$

the prototype function $g(t)$, the emitted signal $s(t)$ and the emitted signal $r(t)$ may be substituted for $x(t)$.

5-3 Modulation algorithm

5-3-1 Principle

25 The baseband signal centered on the frequency $M\nu_0 = f_e/2$, is written as follows:

$$s(t) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} i^{m+n} e^{2i\pi m \nu_0 t} g(t - n\tau_0) \quad (3)$$

$c_{m,n}$

A sample of the signal is therefore written as:

$$s(p \frac{\tau_0}{M}) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} i^{m+n} e^{2i\pi \frac{m p}{2M}} g\left((p - nM) \frac{\tau_0}{M}\right) \quad (4)$$

With the notations introduced here above (formula (2)), we have, after computation:

$$s_p = \sum_n \sum_{m=0}^{2M-1} a_{m,n} i^{m+n} e^{2i\pi \frac{m p}{2M}} (-1)^{mL} g_{p-nM} \quad (5)$$

Given the rapid decrease of the prototype function, only the samples indexed 0 to $2ML-1$ are considered to be non-zero. We should therefore have $0 \leq p - nM \leq 2ML-1$. Taking $p = k + jM$ where $0 \leq k \leq M-1$, we obtain $j - (2L-1) \leq n \leq j$.

The equation (5) becomes:

$$s_{k+jM} = \sum_{n=j-(2L-1)}^j \sum_{m=0}^{2M-1} a_{m,n} i^{m+n} (-1)^{m(n+L)} e^{2i\pi \frac{m(k+(j-n)M)}{2M}} g_{k+(j-n)M} \quad (6)$$

Finally, assuming $q = j - n$, we obtain the formula from which we derive the modulation algorithm:

$$s_{k+jM} = \sum_{q=0}^{2L-1} \sum_{m=0}^{2M-1} a_{m,(j-q)} i^{m+(j-q)} (-1)^{m(j-q+L)} e^{2i\pi \frac{m(k+qM)}{2M}} \cdot g_{k+qM}$$

Pre-modulation
Reverse FFT
Weighting by the prototype function g(t)

with $\begin{cases} 0 \leq k \leq M-1 \\ j \in \mathbb{Z} \end{cases}$

(7)

5 Noting $c_{m,j-q}$ as the pre-modulated input values giving:

$$c_{m,j-q} = a_{m,(j-q)} i^{m+(j-q)} (-1)^{m(j-q+L)}$$

the equation (7) becomes:

10

$$s_{k+jM} = \sum_{q=0}^{2L-1} \left(\sum_{m=0}^{2M-1} c_{m,j-q} e^{2i\pi \frac{m(k+qM)}{2M}} \right) g_{k+qM} \quad (8)$$

This formula leads to a modulation algorithm in three main steps:

15

- Pre-modulation of the data elements by means of a simple complex multiplication.
- Reverse Fourier transform (by IFFT algorithm).
- Filtering by the prototype function.

Here, as in the rest of the document, the term filtering is understood to mean an operation of weighting of the results of 2L reverse FFT operations by

certain values of the prototype function, followed by an operation of summing of these weighted coefficients. In other words, this is a linear combination.

Here below, we present two possible modes of implementation. The second mode is optimal and is more precisely the object of the invention.

Although in practice, the work is done at the sample rate τ_0/M , we shall retain the block structure of M samples to describe these modes of implementation with greater clarity.

5-3-2 Direct architecture

In view of the formula (8), it is necessary to perform $2L$ complex IFFT operations with a size $2M$ to generate M samples (corresponding to the duration of a multicarrier symbol τ_0).

However, the result of an IFFT comes into play on the computation of $2L$ consecutive blocks of samples. To compute the M current samples, it is therefore necessary to compute only the reverse Fourier transform of the $2M$ last data elements entered into the modulator, the results of the $2L-1$ other IFFT values having been computed in the previous steps and stored in the memory.

The modulation algorithm therefore comprises the following main steps:

- The pre-modulation of the $2M$ real inputs delivering $2M$ complex values.
- The reverse Fourier transform with a size of $2M$ complex values (IFFT algorithm).
- Storage of the result by re-updating a buffer with a size of $2L*2M$ complex values (containing the results of the $2L$ reverse FFT operations indicated in the computation).
- Filtering of the $2LM$ elements of the storage buffer by the prototype function.
- Sending of the M complex samples thus computed.

The requisite memory size is therefore:

- a RAM with a size of $2L*2M$ complex values (input buffer),

- a ROM with a size of $ML+1$ real values (weighting coefficients).

(The prototype function is chosen to be symmetrical, on the $2ML$ weighting coefficients, and only the $ML+1$ values are distinct.)

This first procedure reveals a waste of RAM type memory. The second
5 architecture proposed shows that it is possible to reduce the size of the necessary RAM by more than half. This reduction is accompanied by a reduction in the number of operations and therefore an increase in the processing speed.

5-3-3 Optimized architecture

It is possible to optimize the architecture of the modulator according to the invention,
10 both at the level of the filtering by the prototype function and that of the reverse FFT. Indeed, in analyzing the formula (8), it can be ascertained that for each of the $2L$ IFFTs involved in the computation of the current block of M samples, only M points on $2M$ are used.

It is then possible to reduce the required RAM type memory by half by storing
15 the data elements used for the computations of the different blocks of samples after filtering, and not before. Furthermore, the specific structure of the complex data elements at input of the reverse FFT ($a_{m,n} (-1)^{m(n+L)} i^{m+n}$) enables the use of a reverse FFT algorithm with real inputs.

In order to specify this method, we shall develop the formula (8):

$$20 \quad s_{k+jM} = \sum_{q'=0}^{L-1} \left[\sum_{m=0}^{2M-1} c_{m,j-2q'} e^{2i\pi \frac{m}{2M} k} g_{k+2q'M} + \sum_{m=0}^{2M-1} c_{m,j-(2q'+1)} e^{2i\pi \frac{m}{2M} (k+M)} g_{k+(2q'+1)M} \right]$$

Let:

$$C_{k,n} = \sum_{m=0}^{2M-1} c_{m,n} e^{2i\pi \frac{m}{2M} k} \quad (9.1)$$

25 and

$$C_{k+M,n} = \sum_{m=0}^{2M-1} c_{m,n} e^{2i\pi \frac{m}{2M} (k+M)} \quad (9.2)$$

We have:

$$s_{k+jM} = \sum_{q'=0}^{L-1} [C_{k,j-2q'} g_{k+2q'M} + C_{k+M,j-(2q'+1)} g_{k+(2q'+1)M}] \quad (10)$$

with $0 \leq k \leq M-1$

- 5 The equation (10) expresses the construction of M complex values from $2ML$ complex values. It can be written more generally:

$$s_{k+jM} = \sum_{q=0}^{2L-1} [\alpha_{k,q} C_{k,j-q} + \beta_{k,q} C_{k+M,j-q}] \quad (11)$$

with $0 \leq k \leq M-1$

- 10 In the embodiment described,

$$\alpha_{k,q} = \begin{cases} 0 & \text{if } q \text{ is odd-parity} \\ g_{k+qM} & \text{if } q \text{ is even-parity} \end{cases} \text{ and } \beta_{k,q} = \begin{cases} g_{k+qM} & \text{if } q \text{ is odd-parity} \\ 0 & \text{if } q \text{ is even-parity} \end{cases}$$

To generate M samples according to this modulation algorithm, it is therefore possible to proceed as illustrated in Figure 1 (step j):

- 15 - Pre-modulation 11 of the $2M$ real inputs.
- Reverse Fourier transform 12 of the $2M$ complex data elements thus obtained so as to generate $C_{k,j}$ and $C_{k+M,j}$.
- A weighting 13 (corresponding to the application of the prototype function) of the result of the reverse Fourier transform by the prototype
- 20 function: L parallel weighting operations.

The L weighting vectors, with a size $2M$, have the following coefficients:

$$[g_0, \dots, g_{2M-1}], [g_{2M}, \dots, g_{4M-1}], \dots, [g_{2LM-2M}, \dots, g_{2LM-1}].$$

- The addition 14 of these weighting results to the output buffer of with a size of $2ML$ complex values
- 25 - The shifting 15 of the output buffer with the sending of M samples,

corresponding to the M oldest values contained in the buffer.

A sample of the signal to be transmitted represents a sum of $2L$ weighted IFFT results. Each block of M consecutive memory slots of the output buffer contains M partial sums of $2L - m_{\text{block}}$ terms each, where m_{block} varies from 1 to $2L$ ($m_{\text{block}} = 2L$ corresponds to the "all at zero" block, due to the buffer shift operation (step 14) at the instant $(j-1)\tau_0$). The $2ML$ elements coming from the L parallel weighting operations are herein added to the $2ML$ elements of the buffer.

After this operation, the M partial sums of the buffer corresponding to $m_{\text{block}} = 1$ are completed, namely the M current samples are computed and may therefore be transmitted.

This operation is described in Figure 2, where $L=4$. Each line illustrates the situation of the construction buffer of the data elements to be transmitted, at a given instant. It is necessary to have $2L$ consecutive symbol times to gradually construct a sample to be transmitted.

The waveform $2L$ shown corresponds to the Iota function. It is represented by the $2L$ vectors of coefficients $[g_k]$ to $[g_{k+7M}]$, where the index k varies from 0 to $M-1$.

At each instant, the $2M$ coefficients at input are multiplied (23) by the coefficients 22 and then added up (24) each to a partial sum.

The M partial sums complemented at the step 15 are transmitted, the contents of the buffer are shifted by M memory slots (so as to ensure the right order of computation of the next M samples) and M zeros are inserted in the M vacant memory slots.

The diagram 25 thus illustrates the computation of S_{k+jM} .

Figure 3 gives a more detailed view of the working of this algorithm for the instants $j-1$ to $j+2$. If we consider the instant j , the coefficient a_{mj} to be transmitted supplies the pre-modulation module 31, which gives the reverse FFT 32 the coefficients c_{mj} . The reverse FFT delivers the C_{kj} and C_{k+Mj} values (the index k varies

from 0 to M-1) subjected to the weighting 33 (the weighting operations in parallel) to deliver the results 34 which are summed up in an output buffer 35.

Figure 3 gives an indication of the exact contents of these output buffers.

Figure 4 illustrates the triggering of this modulation procedure where $L = 4$.

5 The architecture of the modulator corresponding to the above algorithm
presented here above must therefore comprise:

a ROM with a size of $ML+I$ real values containing the coefficients of the filter,

10 a RAM with a size of $2ML$ complex values corresponding to the output buffer,
a complex FFT circuit (achieving a reverse FFT) with a size $2M$.

To increase the processing speed, the weighting operations will be made parallel by using L RAMs with a size $2M$ associated with L multipliers or even $2L$ RAMs with a size of M complex values associated with $2L$ multipliers instead of one RAM with $2ML$ complex values.

15 The complexity of the modulation circuit is therefore:

- for the filtering:

In order to carry out the filtering, we multiply the results of the complex reverse FFT by the $2ML$ coefficients of the prototype function, by carrying out L weighting operations in parallel, including the result of the output buffer. Given that the coefficients of the prototype function are real, we have $(2 \times 2ML)$ real multiplications and $2ML$ complex additions or $4ML$ real additions. The size of the output buffer is then $2ML$ complex memories or $4ML$ real memories.

- for the IFFT transform:

The results indicated in the following table relate to a conventional complex IFFT circuit whose schematic diagram is given in Figure 5. It comprises an input buffer 51, receiving 2M inputs, a computation unit 52 supplied by coefficients stored in the ROM type memory 53 and computed values stored in a RAM type memory 54 that deliver 2M outputs. A control module drives these different elements.

This table gives an estimation of the operations and equipment needed for the modulation part:

Modulation	Addition Operations (real)	Multiplication Operations (real)	RAM (real)	ROM (real)	FIFO (real)
<i>Pre-modulation</i>	×	×	×	×	×
<i>Reverse FFT</i>	$6M(1 + \log_2 M)$	$4M(1 + \log_2 M)$	$8M$	$2M$	×
<i>Filtering</i>	$4ML$	$4ML$	$4ML$	$ML+1$	×

It will be noted that no multiplication or addition is needed for the pre-modulation because the simple complex multiplication to be found at this stage is expressed, at the level of the architecture, by permutations of real and imaginary parts as well as changes of sign.

According to one variant of the invention, an additional gain in memory space may be obtained. It is indeed possible to use only $(2L-1)$ RAMs with M complex values (total storage: $2ML-M$ complex values instead of $2ML$). To do this, at the step j , a reading is done of the M samples to be transmitted into the corresponding RAM gradually, and the M complex values $C_{k+Mj}g_{k+(2L-1)M}$ are written progressively at the same addresses. To carry out this filtering operation, it is possible, as required, to use RAMs or FIFOs.

Figures 6A to 6C illustrate this method in the case where a FIFO structure is chosen.

In the case of Figure 6A, a single multiplier 61 is implemented. It multiplies data elements delivered by the reverse FFT by the weighting coefficients and supplies an adder 62 that also receives the output of the FIFO memory 63 containing $2ML-M$ complex values. This FIFO 63 is supplied by the result of the addition 62. A control module 64 enables the output of the FIFO to be directed outwards to deliver the M complex values ready to be transmitted 65.

It is possible to use N parallel-connected multipliers, where $N = 1, 2, 4, \dots, 2L$.

Thus, in the case of Figure 6B, $L(=4)$ multipliers 61_1 to 61_4 are implemented in parallel. They are supplied alternatively with one or the other of the weighting coefficients associated with them.

5 Each of them supplies an adder 62_1 to 62_4 which also receives data elements from the $2L$ FIFO memories 63_1 to 63_7 each comprising M complex values. The FIFO memory 63_1 delivers the M complex outputs. Selection means 66 enable the selection of a FIFO memory to be taken into account at each point in time.

Figure 6C shows the implementation of $2L (=8)$ multipliers. In this case, the
10 structure no longer requires the presence of control means. The $2L$ FIFO memories 63_1 to 63_7 are each supplied by a multiplier 61_1 to 61_8 , associated with its own weighting coefficient and associated with an adder 62_1 to 62_8 .

It must be noted that the reduction of the memory space needed for the output buffer is valuable only if the following two conditions are met:

15 - the algorithm used to obtain the reverse FFT arranges its output in the optimum order $C_{0,j}, C_{M,j}, C_{1,j}, C_{M+1,j}, \dots, C_{M-1,j}, C_{2M-1}$ and works at the rate $\tau_0/(2M)$.
Indeed, in the case of outputs arranged in the reverse bit order or even in the natural order, $C_{0,j}, C_{1,j}, \dots, C_{2M-2,j}, C_{2M-1,j}$, the proposed gain in memory due to this simultaneous reading and writing of the output buffer then requires the
20 reordering of the outputs of the reverse FFT in the optimum order which requires a storage at output of the FFT. In either case, the gain in memory will be negligible or even zero.

- The multipliers used, to prevent any storage of the outputs of the reverse FFT, work at a high speed: the rate of operation of N parallel-connected
25 multipliers must be equal to $N\tau_0/(2LM)$, for $N = 1, 2, 4, \dots, 2L$.

According to another variant of the invention, it is possible to optimize the reverse FFT. Given the « particular » complex character of the inputs $(a_{m,n}(-1)^{m(n+L)}i^{m+n})$ of the reverse FFT at transmission, it is possible to use an FFT algorithm with real

inputs.

It is known that phase-shifting the inputs x_m of an FFT with a size $2M$, by i^m amounts to applying a circular permutation to its outputs y_k by $M/2$ leftwards. By applying this result, it can be clearly seen that the pre-modulation step:

$$(a_{m,n} i^{m+n} (-1)^{m(n+L)})$$

followed by the complex reverse FFT can be done as illustrated in Figure 7 in the following steps:

- real reverse FFT 71 of the data elements $(-1)^{m(n+L)} a_{m,n}$,
- circular permutation 72 by $M/2$ of the outputs,
- multiplication 73 by i^n .

An algorithm of this kind enables a reduction by half of the memory space needed for the FFT as well as the number of operations. Figure 5 shows these three operations.

It can be noted that the operation of multiplication by $(-1)^{m(n+L)}$ has been omitted. Indeed, it can be avoided.

At transmission, to generate the baseband signal $s(t)$ (equation 1) digitally, the values of $a_{m,n}$ must be multiplied by $(-1)^{m(n+L)}$. In reception, the estimation of the data requires this multiplication again as shall be seen hereinafter.

Given the fact that the withdrawal of this multiplier term has no effect on the orthogonality of the time-frequency translated values, it is possible to remove the need for this multiplication. This amounts then to generating the baseband signal centered on the frequency $Mv_0 = f_c/2$ according to:

$$s(t) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} (-1)^{m(n+L)} e^{i\varphi_{m,n}} e^{2i\pi m v_0 t} g(t - n\tau_0).$$

6 - Demodulation

The method of demodulation must enable a recovery of the useful information transmitted through the samples of the signal received in reception. It is assumed

here that the "Doppler-delay" channel (the most general case) of the transfer function $T(f,t)$ is perfectly estimated and that it is locally likened to a complex multiplier channel $T_{m,j} = \rho_{m,j} e^{i\theta_{m,j}}$.

Given the orthogonality of the "time-frequency" translated functions of the prototype function, the information sent at the instant $j\tau_0$, on the carrier m is thus estimated:

$$\hat{a}_{m,j} = \Re \left[\frac{1}{\rho_{m,j}} e^{-i\theta_{m,j}} \int r(t) g_{m,j}^*(t) dt \right] \quad (12)$$

In practice, we work on the versions sampled at $\frac{\tau_0}{M} = \frac{1}{W}$ of the received signal, the demodulation function then becomes:

$$\hat{a}_{m,j} \approx \Re \left[\frac{1}{\rho_{m,j}} e^{-i\theta_{m,j}} (-i)^{m+j} \frac{1}{W} \sum_{p \in \mathbb{Z}} r\left(p \frac{\tau_0}{M}\right) e^{-2i\pi m \frac{p}{2M}} g\left((p-jM) \frac{\tau_0}{M}\right) \right] \quad (13)$$

Resuming the notations given by the formula (2) and taking account of the limited number of coefficients representing the prototype function ($2ML$), we obtain a demodulation formula as follows:

$$\hat{a}_{m,j} \approx \Re \left[\frac{1}{\rho_{m,j}} e^{-i\theta_{m,j}} (-i)^{m+j} (-1)^{m(j+L)} \sum_{k=0}^{2M-1} \left[\sum_{q=0}^{L-1} r_{k+jM+2qM} g_{k+2qM} \right] e^{-2i\pi m \frac{k}{2M}} \right] \quad (14)$$

Phase and amplitude correction Weighting by the prototype function Complex FFT

with $\begin{cases} p = jM + 2qM + k \\ 0 \leq k \leq 2M-1 \\ 0 \leq q \leq L-1 \end{cases}$

The formula (14) suggests five steps for the fast demodulation algorithm.:

- weighting of samples received by the prototype function,
- temporal aliasing,
- $2M$ sized complex FFT,
- 5 - phase and amplitude correction,
- extraction of the real part.

The solution proposed according to the invention to minimize the memory space taken up by the filtering (weighting and temporal aliasing) in reception is as follows:

- 10 - inserting the M samples received in an input buffer with a size of $2ML$ complex FFT functions,
- multiplying the data elements of this buffer by the coefficients representing the prototype function,
- summing the results of these multiplications (temporal aliasing),
- 15 - applying a direct Fourier transform to the $2M$ complex values thus obtained,
- correcting the result of this FFT in phase and amplitude,
- extracting the real part.

It must be noted that this technique is independent of the way in which the signal has been constructed at transmission. It can be applied to the reception of any
20 type of OFDM/OQAM multicarrier signal.

In order to illustrate the working of this algorithm, we shall break down the complex $2M$ sized complex signals into two M sized complex sub-signals each, as follows:

$$r_{k+jM+2qM} = r_{k'+jM+2qM} \times 1_{\{k \in \{0, \dots, M-1\}\}} + r_{(k'+M)+jM+2qM} \times 1_{\{k \in \{M, \dots, 2M-1\}\}} \quad (15.1)$$

25 with $\begin{cases} 0 \leq k \leq 2M-1 \\ 0 \leq k' \leq M-1 \end{cases}$

and

$$g_{k+jM+2qM} = g_{k'+jM+2qM} \times 1_{\{k \in \{0, \dots, M-1\}\}} + g_{(k'+M)+jM+2qM} \times 1_{\{k \in \{M, \dots, 2M-1\}\}}$$

with $\begin{cases} 0 \leq k \leq 2M-1 \\ 0 \leq k' \leq M-1 \end{cases}$ (15.2)

The entry of FFT for its part will be referenced $R_{k,j} = \sum_{q=0}^{L-1} r_{k+jM+2qM} \cdot g_{k+2qM}$, k

going from 0 to 2M-1.

- 5 The estimation of the data elements sent will start after a delay of $(2L-1)\tau_0$. It is necessary indeed that all the received samples comprising the data element $a_{m,j}$ should be stored in the input buffer before $\hat{a}_{m,j}$ is computed.

The notations (15.1) and (15.2) here above make it possible, when $L=4$, the inputs of the FFT needed for the estimation of $a_{m,0}$, to write these equations in the

10 form (with $k' = 0 \dots M-1$):

$$R_{k',0} = r_{k'}g_{k'} + r_{k'+2M}g_{k'+2M} + r_{k'+4M}g_{k'+4M} + r_{k'+6M}g_{k'+6M}$$

$$R_{k'+M,0} = r_{k'+M}g_{k'+M} + r_{k'+3M}g_{k'+3M} + r_{k'+5M}g_{k'+5M} + r_{k'+7M}g_{k'+7M}$$

- Similarly, the inputs of the FFT corresponding to the estimation of the values
- 15 $a_{m,1}$ ($m=0$ to $2M-1$) are thus built:

$$R_{k',1} = r_{k'+M}g_{k'} + r_{k'+3M}g_{k'+2M} + r_{k'+5M}g_{k'+4M} + r_{k'+7M}g_{k'+6M}$$

$$R_{k'+M,1} = r_{k'+2M}g_{k'+M} + r_{k'+4M}g_{k'+3M} + r_{k'+6M}g_{k'+5M} + r_{k'+8M}g_{k'+7M}$$

...

- Figure 8 illustrates the working of the architecture proposed in the case where $L=4$. The general case is illustrated by Figure 9 and is deduced directly from Figure
- 20 8.

In this figure 8, the M samples 81 received at an given point in time are stored in an input buffer 82. At each symbol time, the data elements contained in this buffer 82 are multiplied (83) by the weighting coefficients 84 representing the waveform 85 (IOTA in the example) then added up (86) to carry out the aliasing.

- 25 The corresponding data elements $R_{k,j}$ supply the FFT 87, performed on 2M

complex samples. Then a phase correction 88 is done and then an extraction 89 of the real part.

Finally, a shift is made of the contents of the input buffer 82. Figure 8 presents the contents of this buffer for eight successive instants, corresponding to the production of the outputs \hat{a}_{mj} à \hat{a}_{mj+7} .

The above formulae represent the case of the demodulator associated with an OFDM/OQAM modulator with a density 2. However, this architecture remains applicable to the case of the restitution of $2M$ complex values from M complex values resulting from the general case of modulation illustrated by the formula (11). The associated general formula would be:

$$\begin{cases} R_{k',j} = \sum_{q'=0}^{2L-1} r_{k',j+q'} \cdot \alpha'_{k',q'} \\ R_{k'+M,j} = \sum_{q'=0}^{2L-1} r_{k',j+q'} \cdot \beta'_{k',q'} \end{cases} \quad \text{with } k' \in \{0, \dots, M-1\} \quad (16)$$

The above algorithm requires the following means:

- a RAM with a size of $2ML$ complex values (input buffer),
- a ROM with a size of $(ML+1)$ real values (coefficients of the digital filter),
- 1, L or $2L$ complex multipliers depending on the degree of parallel performance of the weighting operations,
- a complex FFT circuit with a size $2M$.

Figure 10 illustrates the architecture proposed.

The input buffer, capable of containing $2ML$ complex values, receives M samples at each τ_0 . The weighting by the prototype function is done by the multiplication operations 102 and then the aliasing is done by means of two adders 103_1 and 103_2 , which supply a buffer 104 of $2M$ values supplying the complex FFT 105.

At the end of the FFT operation 105, a phase and amplitude correction 106 is

Just as at transmission, it is possible to perform the weighting operations in parallel (complex multiplication) by using $2L$ buffers with a size of M complex values associated with L , or $2L$ multipliers, rather than a single one with a size of $2ML$. These aspects are illustrated respectively by Figures 11 and 12. The operation is deduced directly from the one described with reference to Figures 6B and 6C for transmission.

To perform this operation, it is possible, as needed, to use RAMs or FIFO memories. Figures 11 and 12 implement this method in the case of a FIFO structure.

20

- the algorithm used to achieve the FFT works at the rate $\tau_0/(2M)$ with the inputs arriving in the « optimum » order $R_{0,j}, R_{M,j}, R_{1,j}, R_{M+1,j}, \dots, R_{M-1,j}, R_{2M-1,j}$. If not, a storage at the input of the FFT will be necessary and the memory gain will then be negligible or even zero,
- the multipliers used, also to prevent any storage of inputs of the FFT, work at high speed: the rate of operation of N multipliers in parallel must be equal to $N\tau_0/(2LM)$, for $N = 1, 2, 4, \dots, 2L$.

CLAIMS

1. Method for the modulation of a multicarrier signal with a density $1/(v_0 \cdot \tau_0) = 2$, formed by successive symbols, each comprising M samples to be transmitted and constituted by a set of 2M orthogonal carrier frequencies in the real sense,
the interval between two neighboring carrier frequencies being equal to v_0 and the interval between the times of transmission of two consecutive symbols, or the symbol time, being equal to τ_0 ,
each of said carrier frequencies being modulated according to one and the same modulation prototype function $g(t)$ with a truncation length of $2L\tau_0$,
characterized in that it comprises, at each symbol time, the following steps:
 - the obtaining of a set of 2M complex coefficients representing data to be transmitted;
 - the computing of 2LM linear combinations from said 2M complex coefficients obtained, the weighting coefficients used in these combinations representing said prototype function $g(t)$, so as to obtain 2LM coefficients;
 - the summing of said 2LM coefficients weighted in the predetermined storage locations of a memory comprising 2LM storage locations representing 2L groups of M distinct partial sums,
so as to gradually form, in said storage locations, over a duration of $2L\tau_0$, M samples to be transmitted;
 - the transmission of said samples to be transmitted.
2. Method of modulation according to claim 1, characterized in that a sample to be transmitted at the instant $j\tau_0 + k\tau_0/M$, referenced s_{k+jM} is written as follows:

$$s_{k+jM} = \sum_{q=0}^{2L-1} [\alpha_{k,q} C_{k,j-q} + \beta_{k,q} C_{k+M,j-q}]$$

where: $C_{0,j}$ to $C_{2M-1,j}$ are the 2M complex coefficients generated between the instants

$j\tau_0$ and $(j+1)\tau_0$:

$\alpha_{k,q}$ and $\beta_{k,q}$ are said weighting coefficients.

3. Method of modulation according to claim 2, characterized in that:

- $\alpha_{k,q} = 0$ for q as an odd parity number;

5 - $\beta_{k,q} = 0$ for q as an even parity number.

4. Method of modulation according to claim 3, characterized in that: it comprises, for the generation of a symbol with an index j formed by M samples, the following steps:

- the obtaining of $2M$ real inputs $a_{m,n}$ representing a source signal;

10 - the pre-modulation of each of said real inputs producing $2M$ complex coefficients;

- the reverse Fourier transform of said $2M$ complex coefficients producing $2M$ complex transformed coefficients $C_{0,j}$ to $C_{2M-1,j}$;

15 - for each of the M pairs $(C_{k,j}, C_{(k+M),j})$ of said transformed coefficients, the computation of $2L$ weighted coefficients, the weighing coefficients representing said prototype function;

- the addition of the result of each of said weighted $2LM$ values to the contents of the $2LM$ distinct memory zones so as to gradually build the samples to be transmitted constituting the symbols $j, (j+1), (j+2), \dots (j+2L-1)$;

20 - the sending of M samples corresponding to the M oldest contents of said memory zones and then the resetting of the contents of said M memory zones.

5. Method of modulation according any of the claims 1 to 4, characterized in that said steps are implemented at the rate τ_0/M of the samples.

25 6. Method of modulation according to any of the claims 1 to 5, characterized in that said transmission step is followed by a step for the updating of said memory locations comprising:

- a physical shifting of the contents of each of said memory locations if the latter are elements of a shift register; or

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7. Method of modulation according to any of the claims 1 to 6, characterized in that said coefficients representing data elements to be transmitted are obtained by the implementation of a mathematical transform comprising the following steps:

- the application of a real reverse Fourier transform;
- the circular permutation of the result of this reverse transform by $M/2$ coefficients leftwards;
- the multiplication of each of said coefficients by i^n .

$$s(t) = \sum_n \sum_{m=0}^{2M-1} a_{m,n} (-1)^{m(n+L)} i^{m+n} e^{2i\pi n \nu_0 t} g(t - n\tau_0)$$

the interval between two neighboring carrier frequencies being equal to ν_0 and the interval between the times of transmission of two consecutive symbols, or the symbol time, being equal to τ_0 ,

- means for the temporary storage of $2M$ groups of M partial sums
- means for the weighting of $2M$ complex coefficients representing data elements to be transmitted by weighting coefficients representing said prototype function $g(t)$

- means for the summing of the weighted coefficients in respective predetermined memory locations of said temporary storage locations,

so as to gradually form said samples to be transmitted on a duration of $2L\tau_0$.

10. Modulation device according to claim 9, characterized in that it comprises:

- means of mathematical transformation delivering said coefficients representing data elements to be transmitted at the rate $\tau_0/2M$ and in the following order $(C_{0,j}, C_{M+1,j}), \dots, (C_{M-1,j}, C_{2M-1,j})$;
- $2LM-M$ simultaneous read/write RAM type memory locations;
- N complex multipliers working at the rate $N\tau_0/2LM$, N being equal to 1, 2, 4, ... or $2L$.

11. Method for the demodulation of a received signal corresponding to a transmitted multicarrier signal with a density $1/(v_0 \cdot \tau_0) = 2$, formed by successive symbols, each comprising M samples to be transmitted and constituted by a set of $2M$ orthogonal carrier frequencies in the real sense, the interval between two neighboring carrier frequencies being equal to v_0 and the interval between the times of transmission of two consecutive symbols, or the symbol time, being equal to τ_0 , each of said carrier frequencies being modulated according to one and the same modulation prototype function $g(t)$ with a truncation length of $2L\tau_0$, characterized in that an estimation of $2M$ real data elements transmitted at a given symbol time is reconstituted by means of the following steps:

- the sampling of said signal received at the sample frequency τ_0/M , delivering M complex samples received;
- the storage of each of said M complex samples received in a predetermined location of an input memory comprising $2ML$ complex locations, in which there have been previously memorized $(2L-1)M$ samples received during the $2l-1$ previous symbol times;
- the multiplication of the $2ML$ values contained in said input memory by coefficients representing said prototype function;

- temporal aliasing, by the summing up of 2M series of L results of multiplication, so as to obtain 2M complex values;
- the processing of said 2M complex values to form said estimations of the 2M real data elements transmitted.

5 12. A demodulation method according to claim 11, characterized in that the 2M complex values derived from the temporal aliasing step between the instants $(j+2L-1)\tau_0$ and $(j+2L)\tau_0$ are written as follows:

$$R_{k',j} = \sum_{q'=0}^{2L-1} \alpha'_{k,q} r_{k'+(j+q')M}$$

$$R_{k'+M,j} = \sum_{q'=0}^{2L-1} \beta'_{k,q} r_{k'+(j+q')M}$$

10

where:

$r_{k'+(j+q')M}$ represents the sample received at the instant $k'\tau_0+(j+q')\tau_0/M$;
 $\alpha'_{k,q}$ and $\beta'_{k,q}$ are said weighting coefficients.

13. Demodulation method according to any of the claims 11 and 12,
 15 characterized in that :

- $\alpha'_{k,q'} = 0$ for q' as an odd parity value;
- $\beta'_{k,q'} = 0$ for q' as an even parity value.

14. Method according to any of the claims 11 to 13, characterized in that said processing step comprises the following steps:

- 20 - the application of a mathematical transformation that is the reverse of the one performed during the modulation on said 2M complex values delivering 2M transformed values;
- the correction of phase and/or amplitude distortions due to the transmission channel;
- 25 - the extraction of the real part of said transformed complex values.

15. Demodulation method according to any of the claims 11 to 14,

characterized in that said steps are implemented at the rate τ_0/M of the samples.

16. Device for the demodulation of a received signal corresponding to a transmitted multicarrier signal with a density $1/(v_0 \cdot \tau_0) = 2$, formed by successive symbols, each comprising M samples to be transmitted and constituted by a set of 2M

5 orthogonal carrier frequencies in the real sense,

the interval between two neighboring carrier frequencies being equal to v_0 and the interval between the times of transmission of two consecutive symbols, or the symbol time, being equal to τ_0 ,

each of said carrier frequencies being modulated according to one and the same modulation prototype function $g(t)$ with a truncation length of $2L\tau_0$,
10 characterized in that it comprises:

- means for the sampling of said received signal;
- means for the temporary storage of the complex sample functions comprising 2ML complex locations;
- 15 - means for the multiplication of said memorized samples by weighting coefficients representing said prototype function;
- temporal aliasing means summing up L weighting results so as to obtain 2M complex values;
- means for the processing of said complex values delivering an estimation of 2M real data elements transmitted at each symbol time.
- 20

17. Demodulation device according to claim 16, characterized in that it comprises:

- means of mathematical transformation that is the reverse of the transformation performed during the modulation on said 2M complex values;
- 25 - means for the correction of phase and/or amplitude distortions due to the transmission channel;
- means for the extraction of the real part of said transformed complex values

18. Demodulation device according to any of the claims 16 and 17,

- storage means comprising 2ML-M simultaneous write/read RAM type complex memory locations;

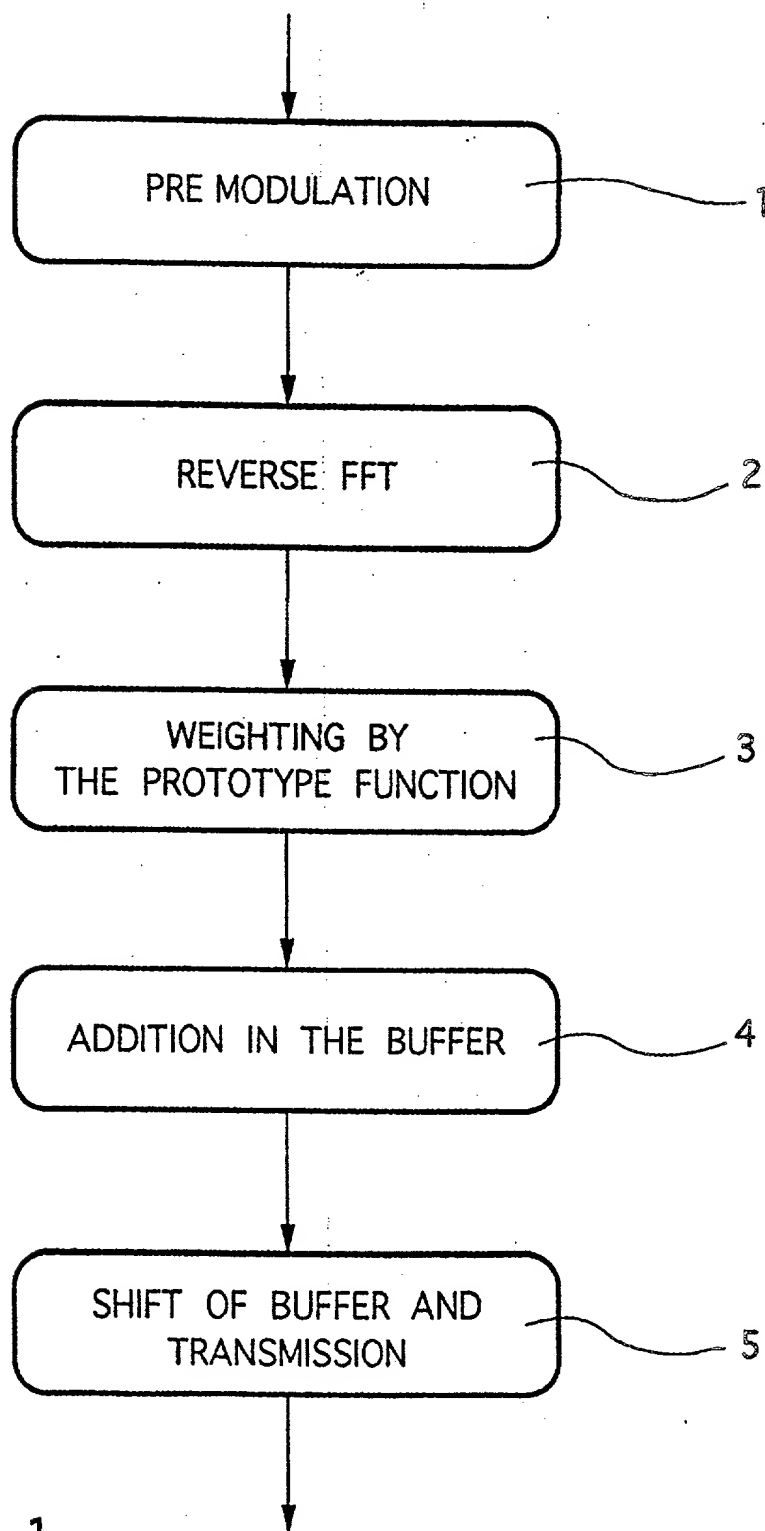
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Fig. 1

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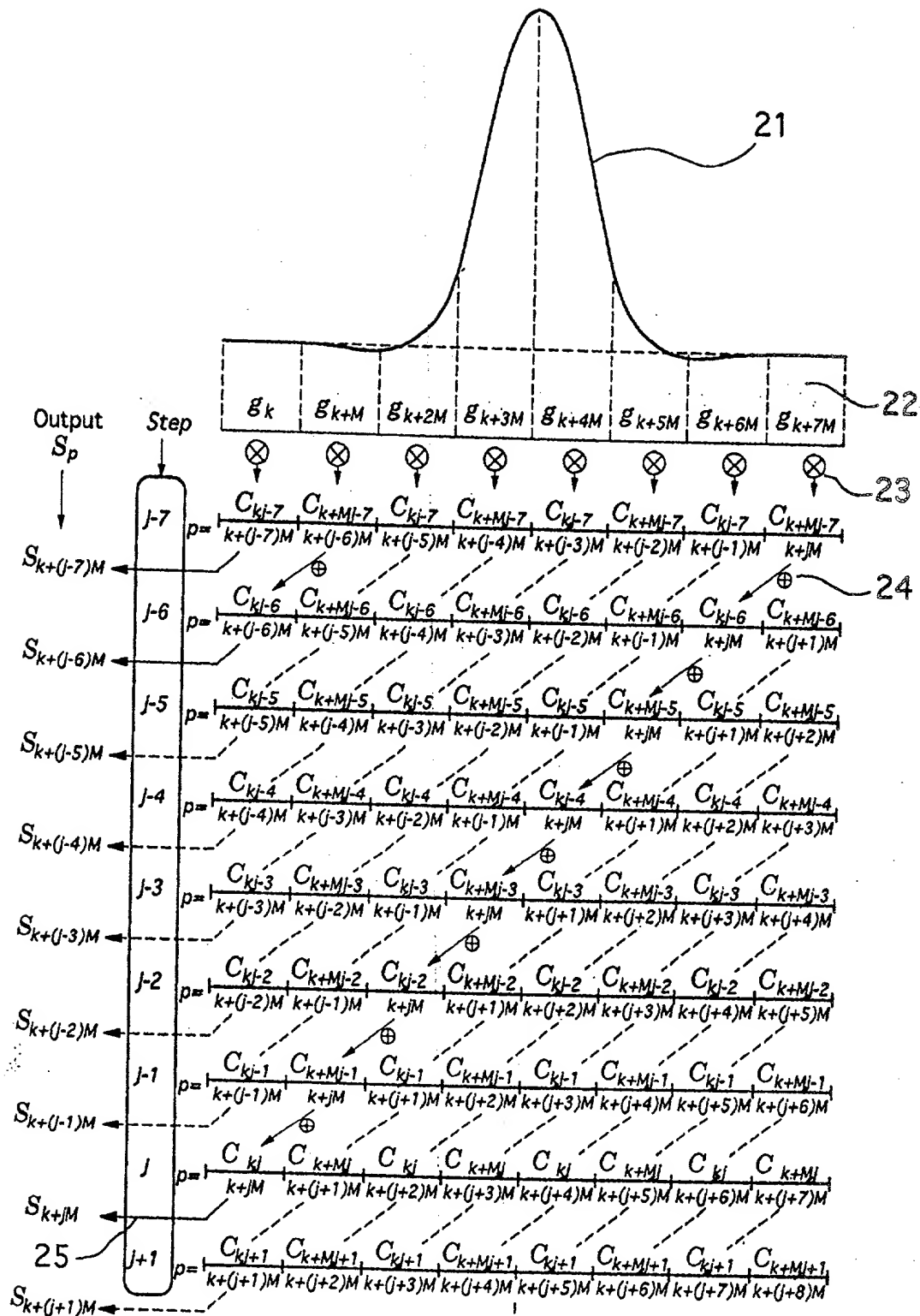


Fig. 2

Fig. 3

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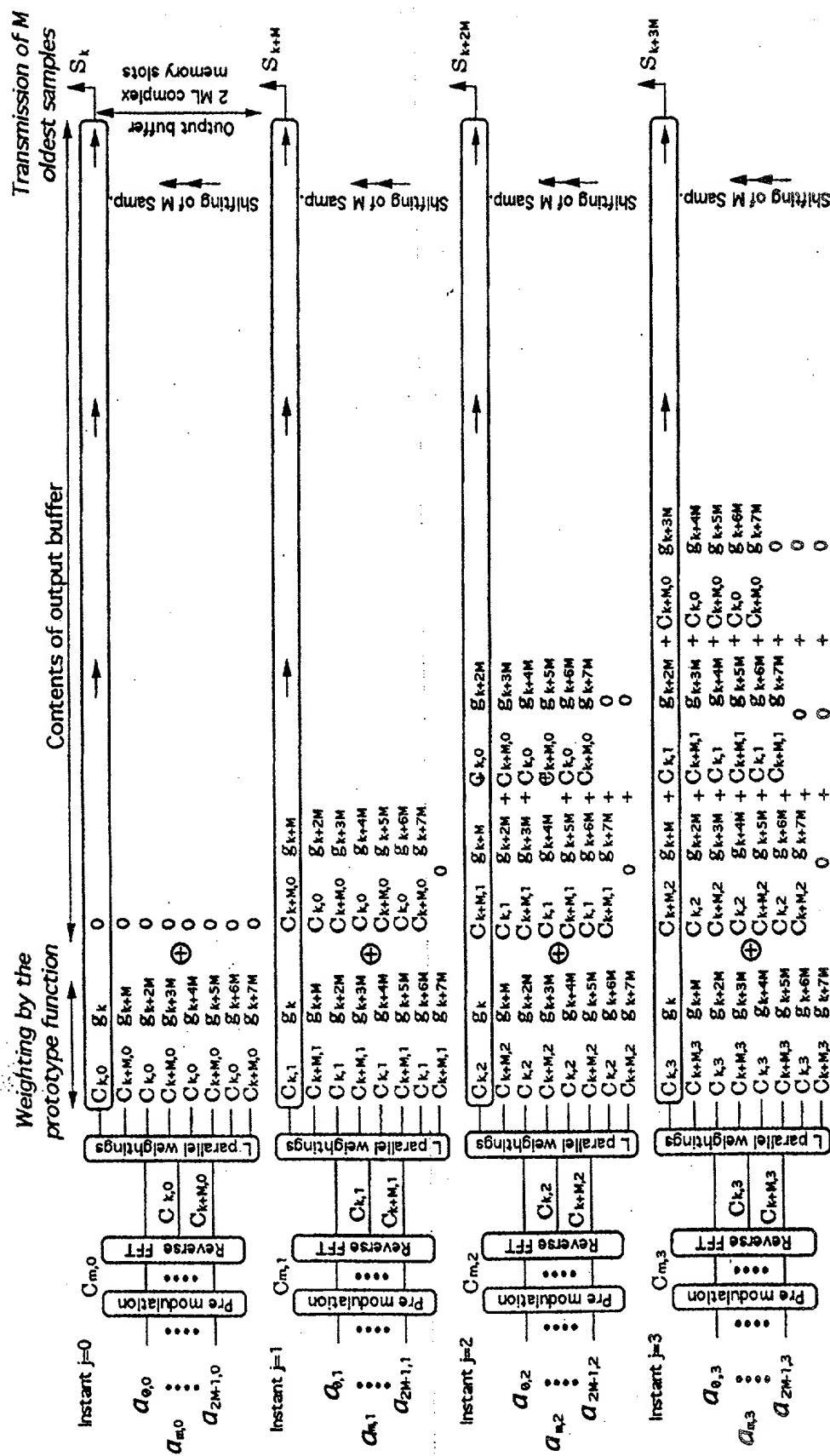


Fig. 4

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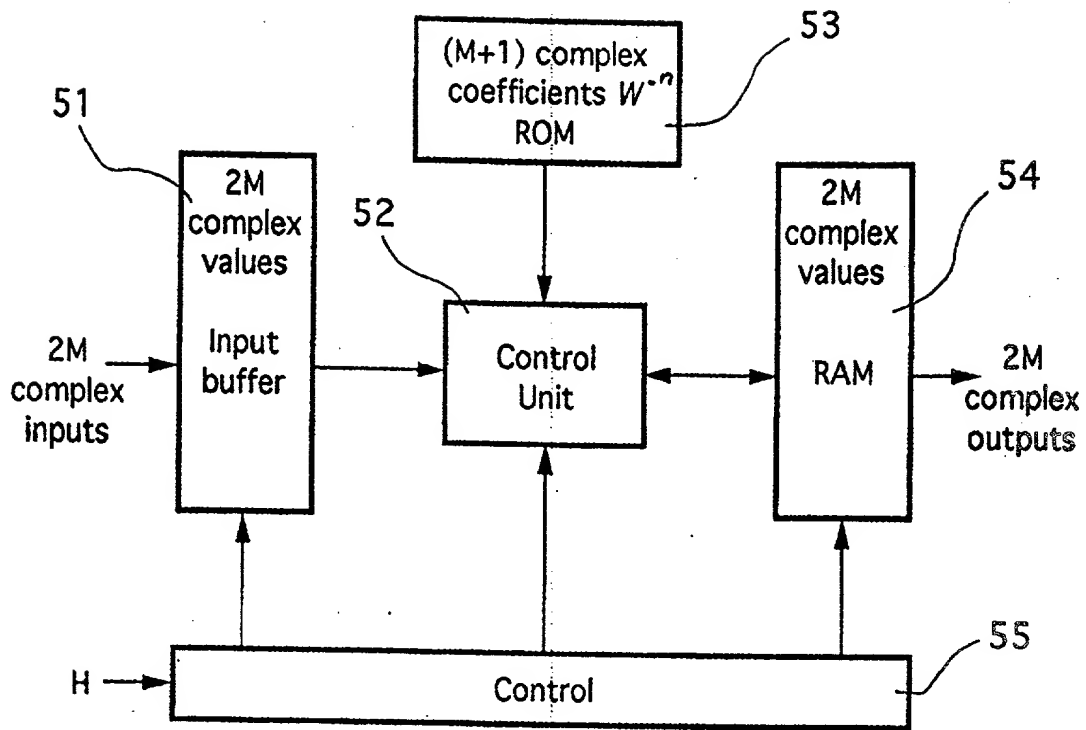


Fig. 5

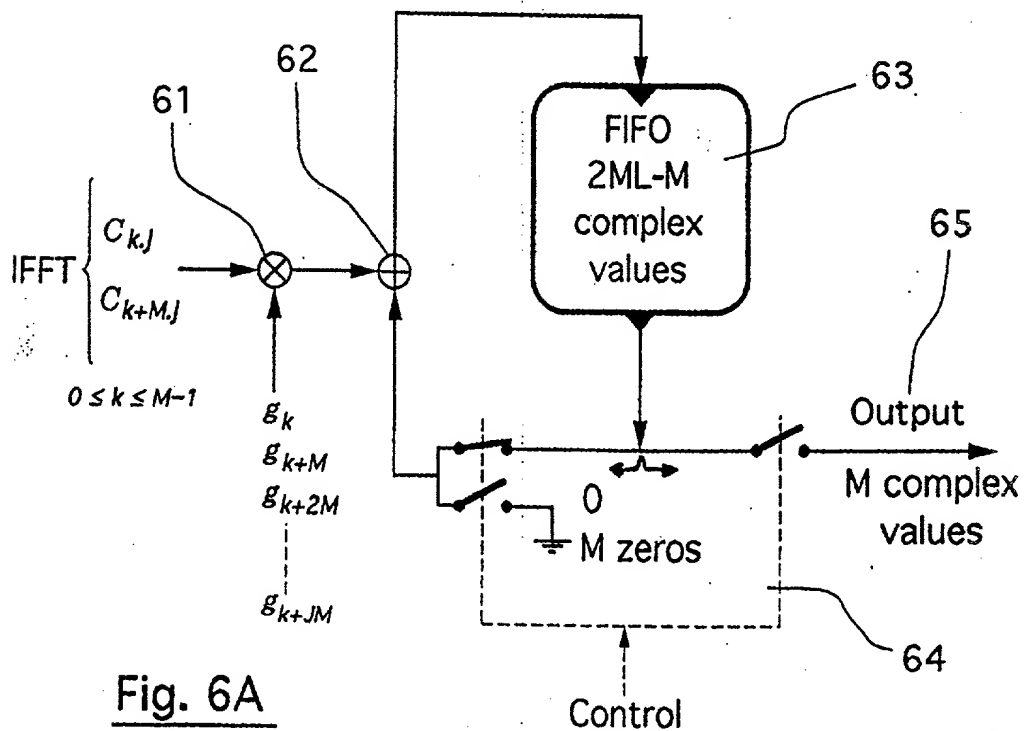
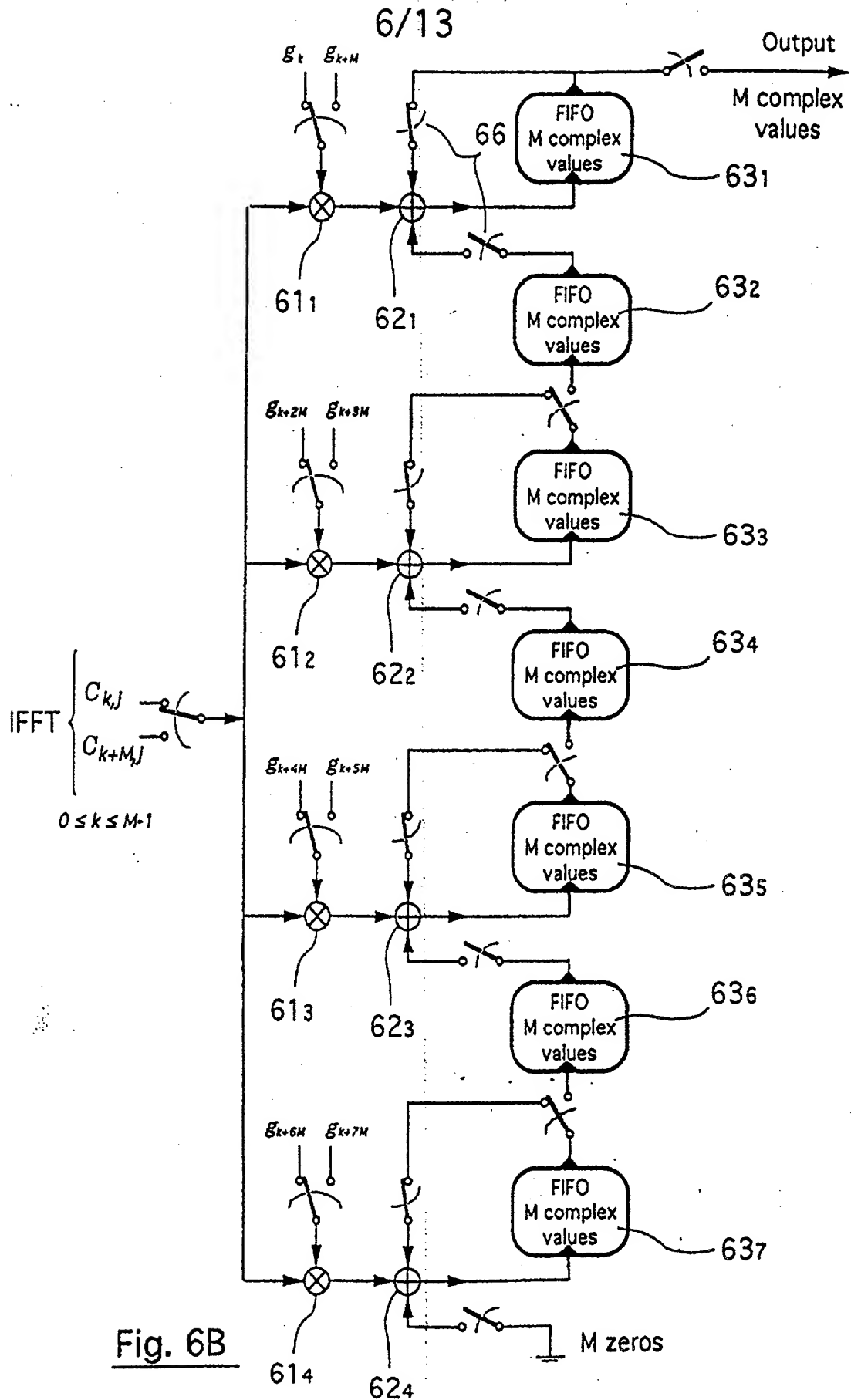
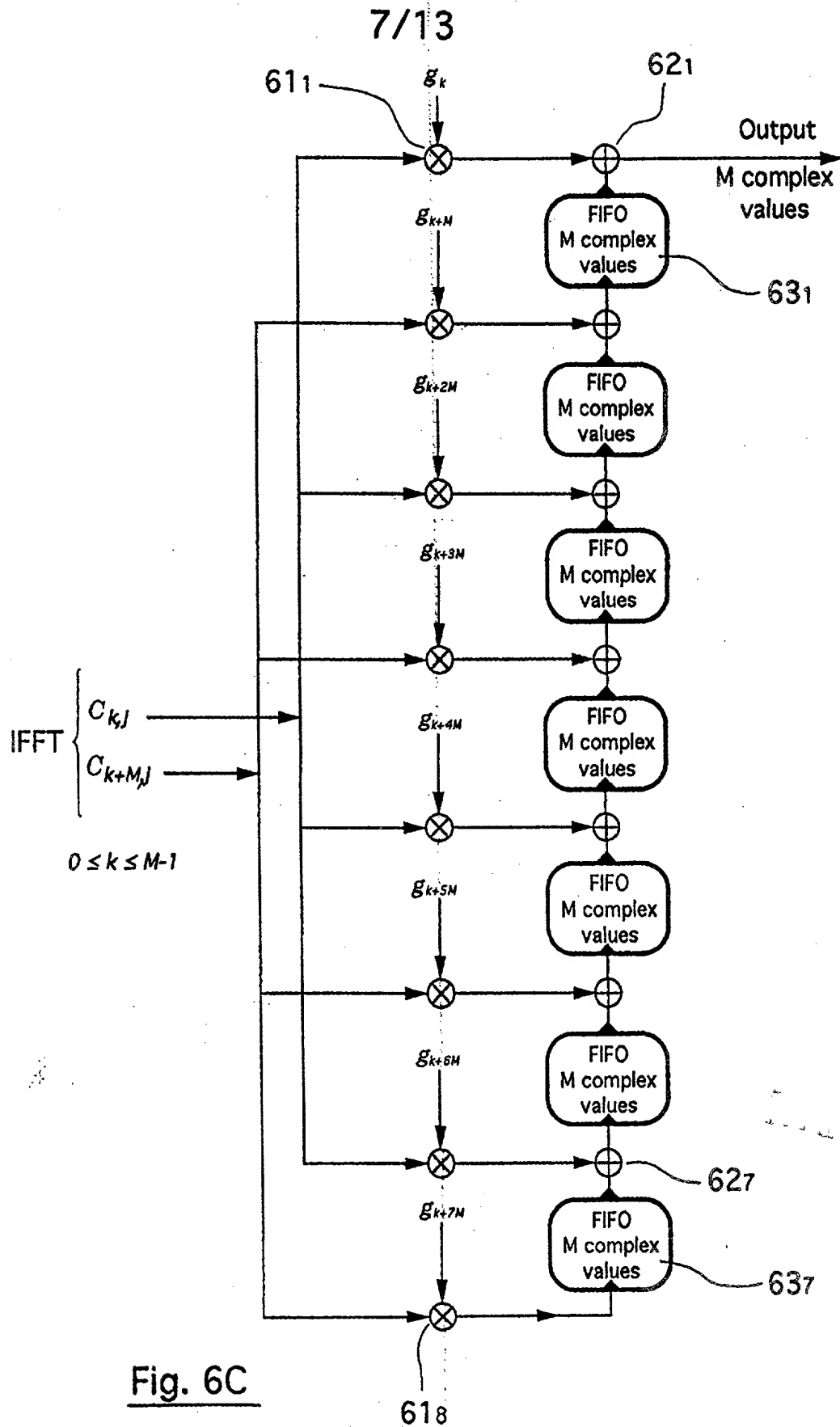


Fig. 6A





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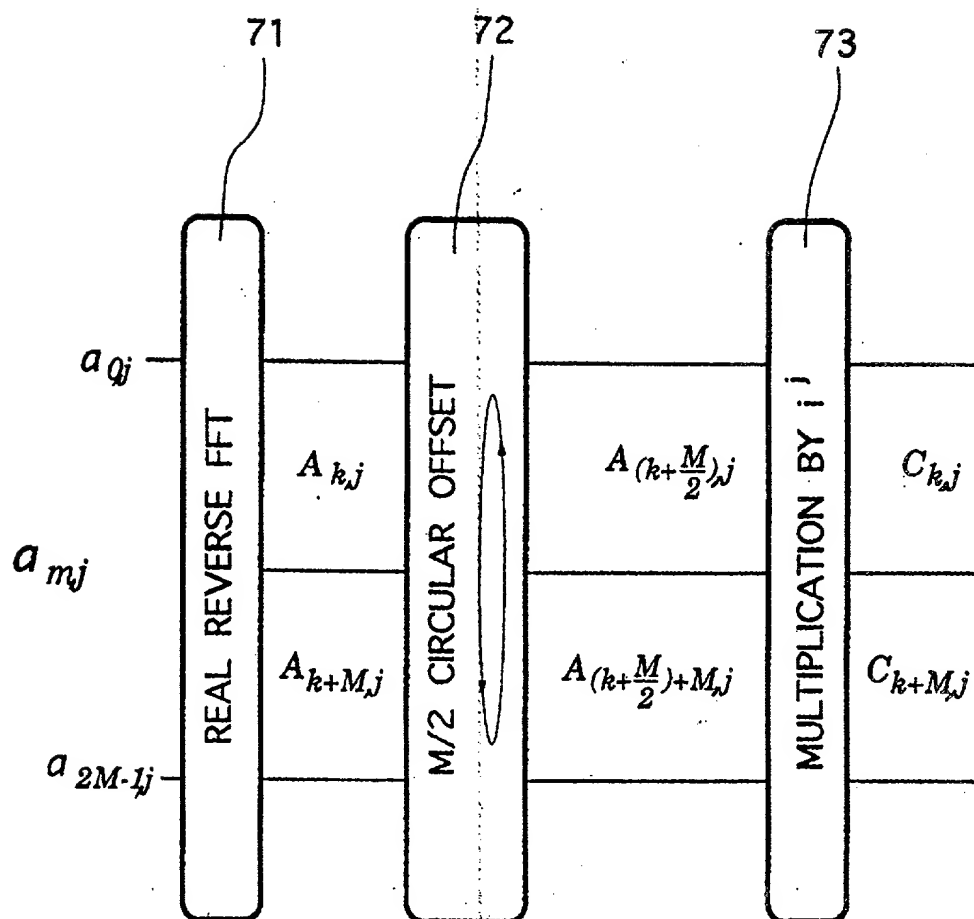
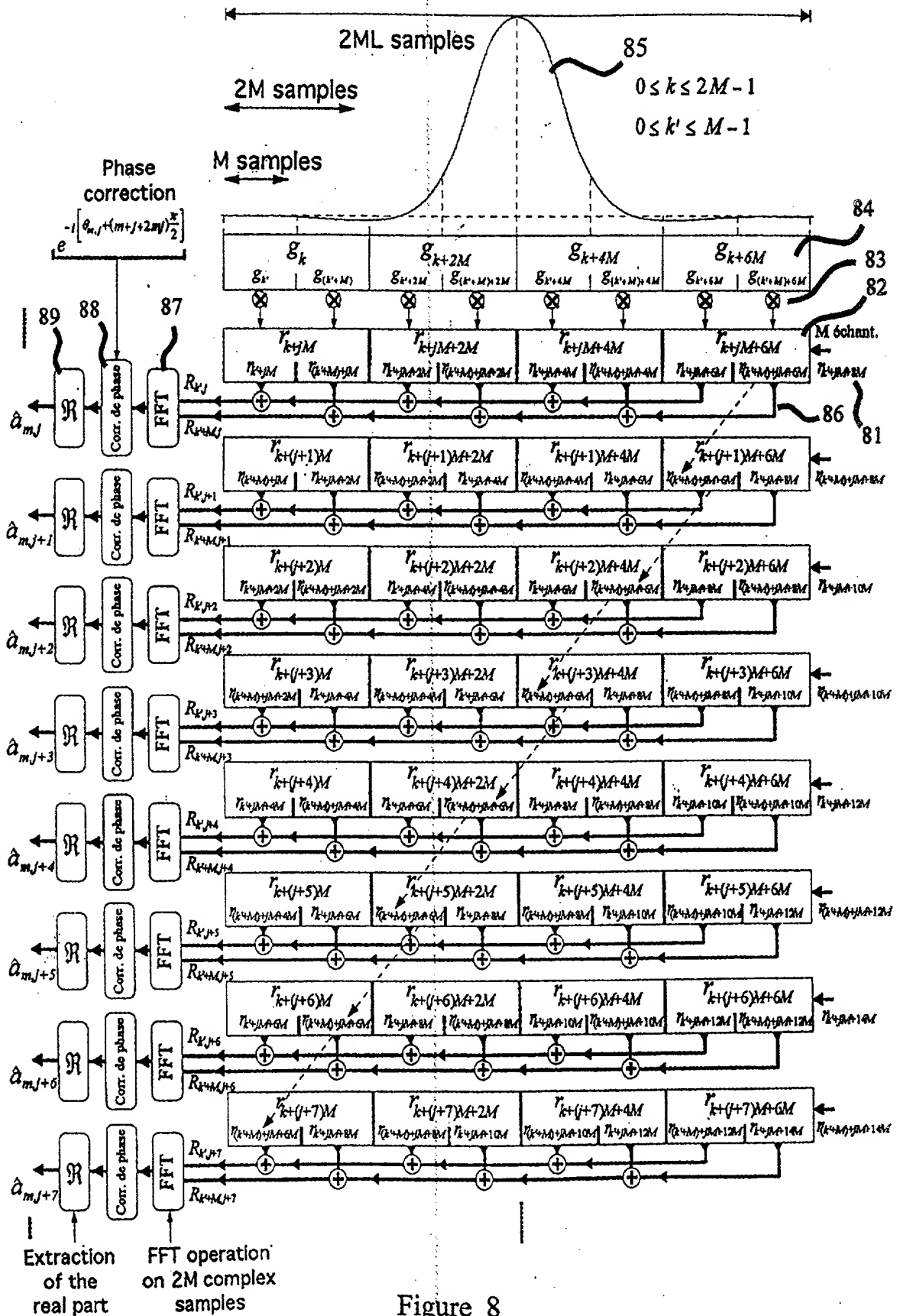
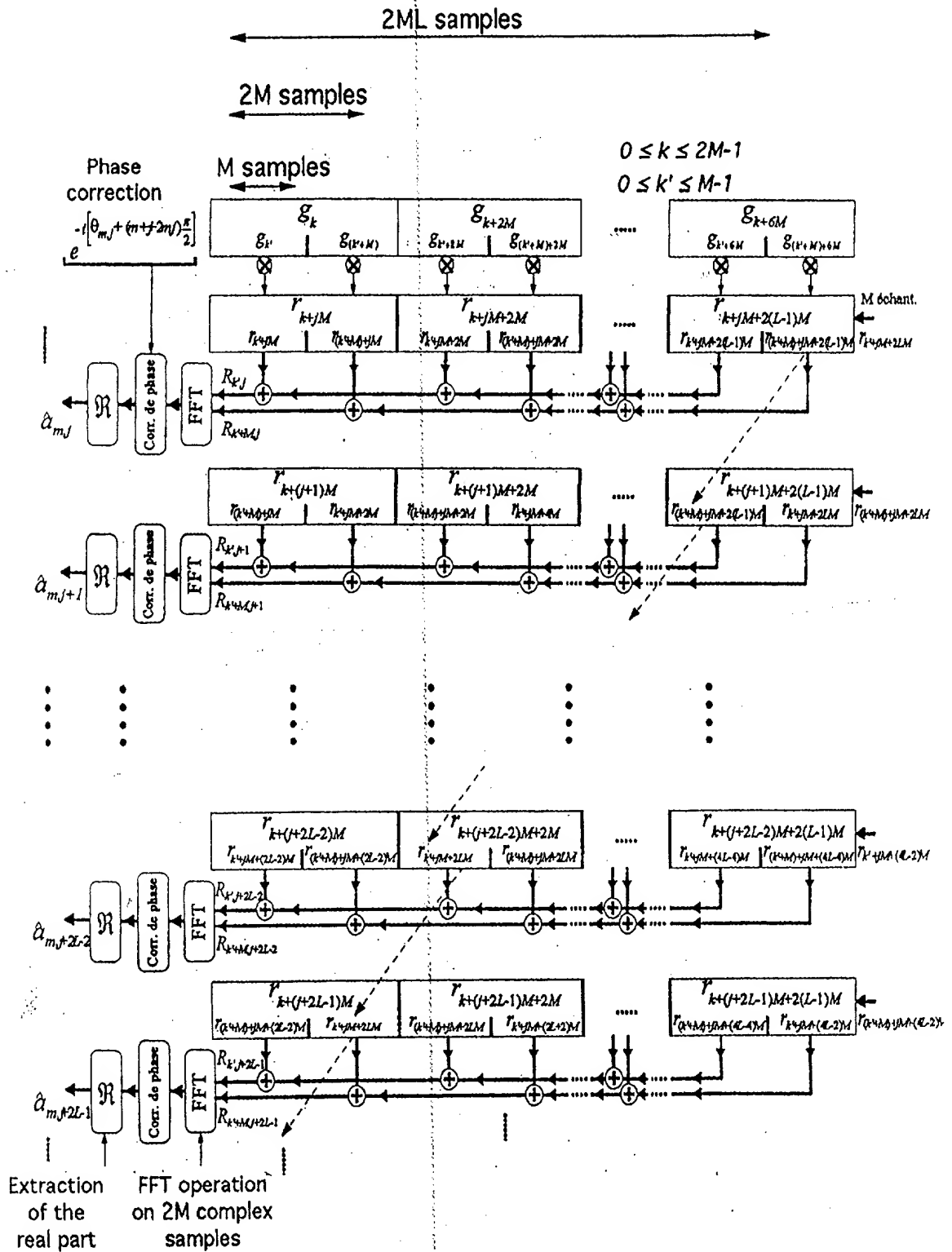


Fig. 7

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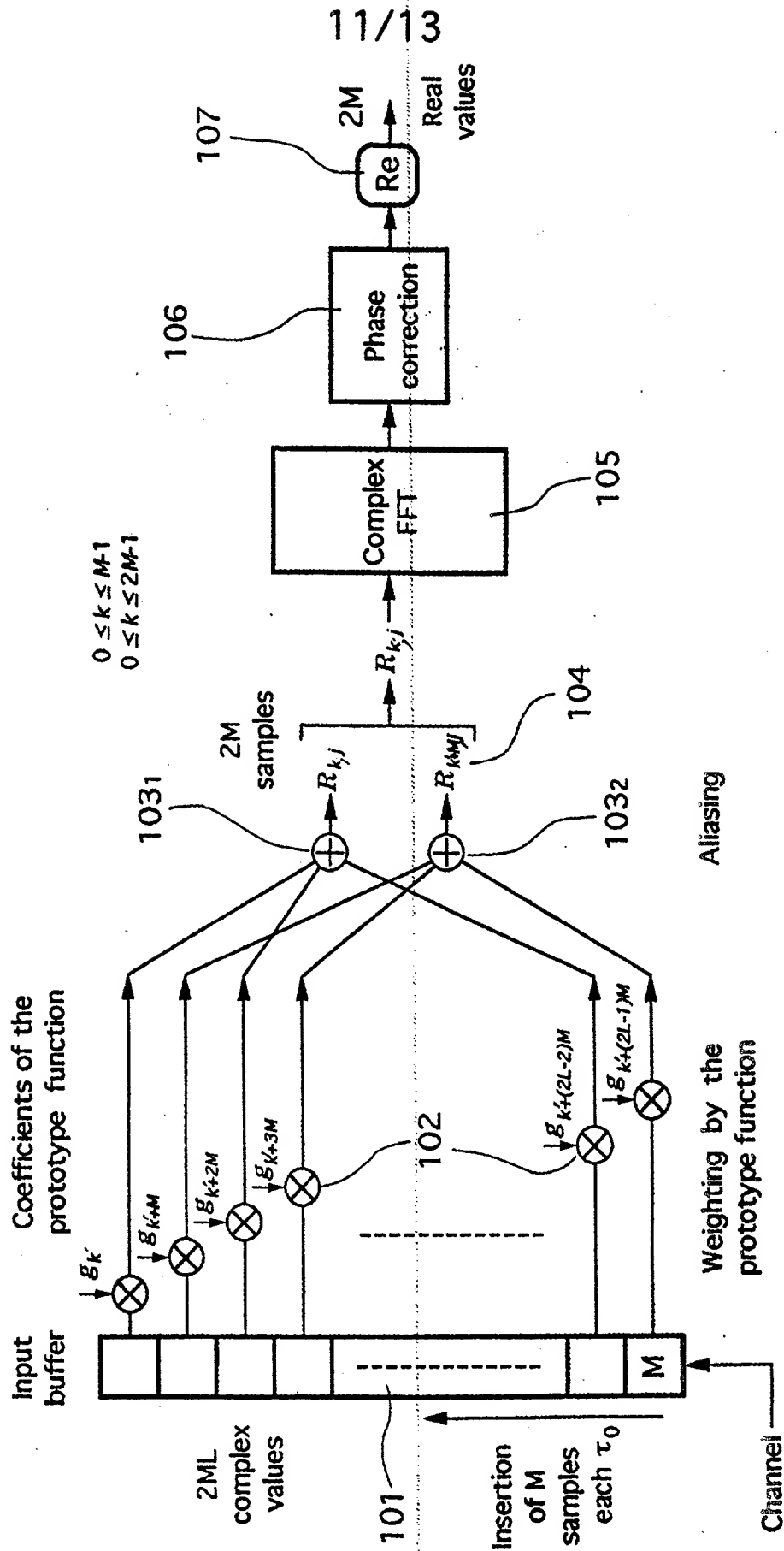


Fig. 10

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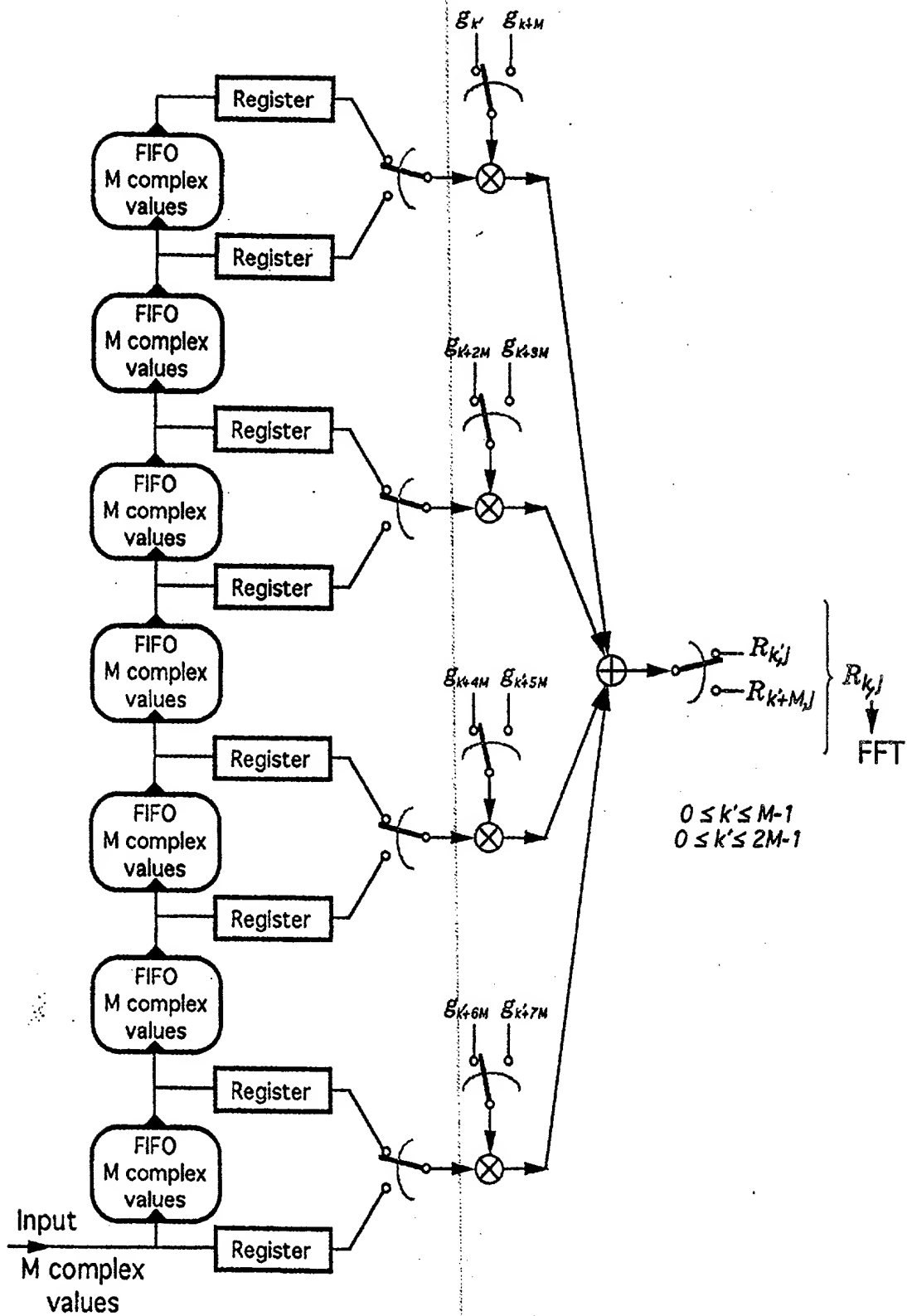


Fig. 11

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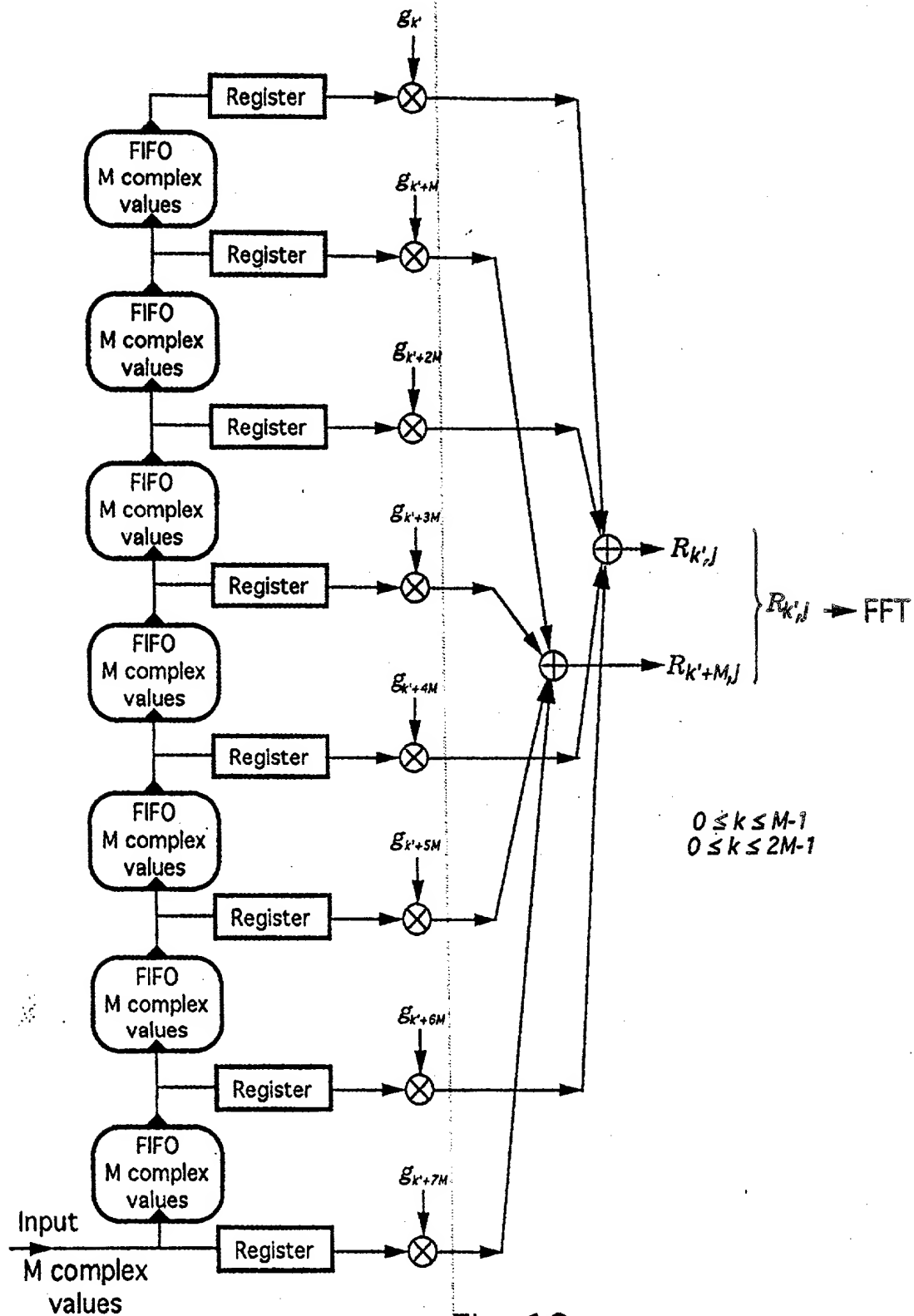


Fig. 12

MERCHANT & GOULD P.C.

United States Patent Application

COMBINED DECLARATION AND POWER OF ATTORNEY

As a below named inventor I hereby declare that: my residence, post office address and citizenship are as stated below next to my name; that

I verily believe I am the original, first and sole inventor (if only one name is listed below) or a joint inventor (if plural inventors are named below) of the subject matter which is claimed and for which a patent is sought on the invention entitled: MULTICARRIER MODULATION USING WEIGHTED PROTOTYPE FUNCTIONS

The specification of which

- a. ☐ is attached hereto
b. ☒ was filed on December 29, 1999 as application serial no. and was amended on (if applicable) (in the case of a PCT-filed application) described and claimed in international no. PCT/FR98/01398 filed June 30, 1998 and as amended on (if any), which I have reviewed and for which I solicit a United States patent.

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to the patentability of this application in accordance with Title 37, Code of Federal Regulations, § 1.56 (attached hereto).

I hereby claim foreign priority benefits under Title 35, United States Code, § 119/365 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on the basis of which priority is claimed:

- a. ☐ no such applications have been filed.
b. ☒ such applications have been filed as follows:

FOREIGN APPLICATION(S), IF ANY, CLAIMING PRIORITY UNDER 35 USC § 119			
COUNTRY	APPLICATION NUMBER	DATE OF FILING (day, month, year)	DATE OF ISSUE (day, month, year)
France	FR 97 08547	July 1, 1997	
ALL FOREIGN APPLICATION(S), IF ANY, FILED BEFORE THE PRIORITY APPLICATION(S)			
COUNTRY	APPLICATION NUMBER	DATE OF FILING (day, month, year)	DATE OF ISSUE (day, month, year)

I hereby claim the benefit under Title 35, United States Code, § 120/365 of any United States and PCT international application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, § 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, § 1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application.

U.S. APPLICATION NUMBER	DATE OF FILING (day, month, year)	STATUS (patented, pending, abandoned)

I hereby claim the benefit under Title 35, United States Code § 119(e) of any United States provisional application(s) listed below:

U.S. PROVISIONAL APPLICATION NUMBER	DATE OF FILING (Day, Month, Year)

I hereby appoint the following attorney(s) and/or patent agent(s) to prosecute this application and to transact all business in the Patent and Trademark Office connected herewith:

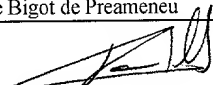

Albrecht, John W.	Reg. No. <u>40,481</u>	Lacy, Paul E.	Reg. No. 38,946
Anderson, Gregg I.	Reg. No. <u>28,828</u>	Larson, James A.	Reg. No. 40,443
Ansems, Gregory M.	Reg. No. <u>42,264</u>	Liepa, Mara E.	Reg. No. 40,066
Batzli, Brian H.	Reg. No. <u>32,960</u>	Lindquist, Timothy A.	Reg. No. 40,701
Beard, John L.	Reg. No. <u>27,612</u>	McDonald, Daniel W.	Reg. No. 32,044
Berns, John M.	Reg. No. <u>43,496</u>	McIntyre, Jr., William F.	Reg. No. P-44,921
Black, Bruce E.	Reg. No. <u>41,622</u>	Mueller, Douglas P.	Reg. No. 30,300
Bruess, Steven C.	Reg. No. <u>34,130</u>	Pauly, Daniel M.	Reg. No. 40,123
Byrne, Linda M.	Reg. No. <u>32,404</u>	Phillips, John B.	Reg. No. 37,206
Carlson, Alan G.	Reg. No. <u>25,959</u>	Plunkett, Theodore	Reg. No. 37,209
Caspers, Philip P.	Reg. No. <u>33,227</u>	Pytel, Melissa J.	Reg. No. 41,512
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Clifford, John A.	Reg. No. <u>30,247</u>	Reiland, Earl D.	Reg. No. 25,767
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Daignault, Ronald A.	Reg. No. <u>25,968</u>	Schuman, Mark D.	Reg. No. 31,197
Daley, Dennis R.	Reg. No. <u>34,994</u>	Schumann, Michael D.	Reg. No. 30,422
Dalglish, Leslie E.	Reg. No. <u>40,579</u>	Scull, Timothy B.	Reg. No. 42,137
Daulton, Julie R.	Reg. No. <u>36,414</u>	Sebald, Gregory A.	Reg. No. 33,280
DeVries Smith, Katherine M.	Reg. No. <u>42,157</u>	Skoog, Mark T.	Reg. No. 40,178
DiPietro, Mark J.	Reg. No. <u>28,707</u>	Soderberg, Richard	Reg. No. P-43,352
Edell, Robert T.	Reg. No. <u>20,187</u>	Stoll-DeBell, Kirstin L.	Reg. No. 43,164
Epp Ryan, Sandra	Reg. No. <u>39,667</u>	Storer, Shelley D.	Reg. No. 45,135
Glance, Robert J.	Reg. No. <u>40,620</u>	Sumner, John P.	Reg. No. 29,114
Goggin, Matthew J.	Reg. No. <u>44,125</u>	Summers, John S.	Reg. No. 24,216
Golla, Charles E.	Reg. No. <u>26,896</u>	Swenson, Erik G.	Reg. No. 45,147
Gorman, Alan G.	Reg. No. <u>38,472</u>	Tellekson, David K.	Reg. No. 32,314
Gould, John D.	Reg. No. <u>18,223</u>	Trembath, Jon R.	Reg. No. 38,344
Gregson, Richard	Reg. No. <u>41,804</u>	Underhill, Albert L.	Reg. No. 27,403
Grisens, John J.	Reg. No. <u>33,112</u>	Vandenburgh, J. Derek	Reg. No. 32,179
Hamre, Curtis B.	Reg. No. <u>29,165</u>	Wahl, John R.	Reg. No. 33,044
Hanson, Randall A.	Reg. No. <u>31,838</u>	Weaver, Karrie G.	Reg. No. 43,245
Holzer, Jr., Richard J.	Reg. No. <u>42,668</u>	Welter, Paul A.	Reg. No. 20,890
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Kadievitch, Natalie D.	Reg. No. <u>34,196</u>	Wickhem, J. Scot	Reg. No. 41,376
Kastelic, Joseph M.	Reg. No. <u>37,160</u>	Williams, Douglas J.	Reg. No. 27,054
Kattelberger, Denise	Reg. No. <u>33,924</u>	Witt, Jonelle	Reg. No. 41,980
Keys, Jeramie J.	Reg. No. <u>42,724</u>	Xu, Min S.	Reg. No. 39,536
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Kowalchyk, Alan W.	Reg. No. <u>31,535</u>		
Kowalchyk, Katherine M.	Reg. No. <u>36,848</u>		

I hereby authorize them to act and rely on instructions from and communicate directly with the person/assignee/attorney/firm/ organization who/which first sends/sent this case to them and by whom/which I hereby declare that I have consented after full disclosure to be represented unless/until I instruct Merchant & Gould P.C. to the contrary.

Please direct all correspondence in this case to Merchant & Gould P.C. at the address indicated below:

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Minneapolis, MN 55402-4131

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

2	Full Name Of Inventor	Family Name Combelles	First Given Name Pierre	Second Given Name M.
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Signature of Inventor 202: 				Date: <i>31 jan 2000</i>
2	Full Name Of Inventor	Family Name Jalali	First Given Name Ali	Second Given Name M.
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pour agir en son (leur) nom auprès des administrations internationales compétentes en ce qui concerne la demande internationale relative à [titre de l'invention, cote du dossier du déposant ou du mandataire, si elle a été indiquée dans la requête, numéro de la demande internationale, s'il est déjà disponible] :

**“Procédé et dispositif de modulation d'un signal multiporteuse de type
 OFMD/OQAM, et dispositif de démodulation correspondant”**

4246.WOdéposée auprès de [nom de l'office] **INPI RENNES**

en tant qu'office récepteur et pour faire ou recevoir des paiements en son (leur) nom.

Lieu :

Date :

Signatures du déposant et des inventeurs (s'il y en a plusieurs, tous doivent signer) :

FRANCE TELECOM
TELEDIFFUSION DE FRANCE

COMBELLES
Pierre

LACROIX
Dominique

JALALI
Ali

§ 1.56 Duty to disclose information material to patentability.

(a) A patent by its very nature is affected with a public interest. The public interest is best served, and the most effective patent examination occurs when, at the time an application is being examined, the Office is aware of and evaluates the teachings of all information material to patentability. Each individual associated with the filing and prosecution of a patent application has a duty of candor and good faith in dealing with the Office, which includes a duty to disclose to the Office all information known to that individual to be material to patentability as defined in this section. The duty to disclose information exists with respect to each pending claim until the claim is canceled or withdrawn from consideration, or the application becomes abandoned. Information material to the patentability of a claim that is canceled or withdrawn from consideration need not be submitted if the information is not material to the patentability of any claim remaining under consideration in the application. There is no duty to submit information which is not material to the patentability of any existing claim. The duty to disclose all information known to be material to patentability is deemed to be satisfied if all information known to be material to patentability of any claim issued in a patent was cited by the Office or submitted to the Office in the manner prescribed by §§ 1.97(b)–(d) and 1.98. However, no patent will be granted on an application in connection with which fraud on the Office was practiced or attempted or the duty of disclosure was violated through bad faith or intentional misconduct. The Office encourages applicants to carefully examine:

- (1) prior art cited in search reports of a foreign patent office in a counterpart application, and
- (2) the closest information over which individuals associated with the filing or prosecution of a patent application believe any pending claim patentably defines, to make sure that any material information contained therein is disclosed to the Office.

(b) Under this section, information is material to patentability when it is not cumulative to information already of record or being made of record in the application, and

- (1) It establishes, by itself or in combination with other information, a prima facie case of unpatentability of a claim;
- (2) It refutes, or is inconsistent with, a position the applicant takes in:
 - (i) Opposing an argument of unpatentability relied on by the Office, or
 - (ii) Asserting an argument of patentability.

A prima facie case of unpatentability is established when the information compels a conclusion that a claim is unpatentable under the preponderance of evidence, burden-of-proof standard, giving each term in the claim its broadest reasonable construction consistent with the specification, and before any consideration is given to evidence which may be submitted in an attempt to establish a contrary conclusion of patentability.

(c) Individuals associated with the filing or prosecution of a patent application within the meaning of this section are:

- (1) Each inventor named in the application;
- (2) Each attorney or agent who prepares or prosecutes the application; and
- (3) Every other person who is substantively involved in the preparation or prosecution of the application and who is associated with the inventor, with the assignee or with anyone to whom there is an obligation to assign the application.

(d) Individuals other than the attorney, agent or inventor may comply with this section by disclosing information to the attorney, agent, or inventor.